



DIP LOG CALCULATIONS

COMPANY REICHHOLD ENERGY CORPORATION

WELL CROWN ZELLERBACH 22-6 REDRILL NO. 1

FIELD MIST NEHALEM BASIN

COUNTY COLUMBIA STATE OREGON

WELEX

A **Halliburton** Company



American Company

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CORRELATION INTERVAL	CORR. GRADE	DIP ANG.	DIP AZ.	DRIFT ANG.	DRIFT AZ.	NO.1	DIA 13	DIA 24	DISPLACEMENTS					M	
									H12	H23	H13	H24	H14		
578.0	580.0	C	46.4	127	2.9	345	34	6.8	7.0	-3.4		-.2		3.4	0
583.0	585.0	C	48.0	148	3.0	350	30	6.6	6.7	-3.9		-3.0		2.1	0
606.0	608.0	C	21.4	106	2.7	348	329	6.6	6.9	-1.4		-1.6		.5	0
611.0	613.0	B	44.9	123	2.8	348	321	6.6	6.9	-3.9		-5.8		-1.7	0
631.0	633.0	B	43.2	115	2.6	339	294	6.6	6.9	-2.8		-5.8		-2.7	0
633.0	635.0	C	45.6	123	2.6	341	294	6.6	6.9	-2.9		-6.2		-3.6	0
636.0	638.0	B	43.9	116	2.6	341	291	6.5	6.9	-2.8		-5.9		-3.1	0
638.0	640.0	B	46.8	116	2.6	341	292	6.5	6.9	-2.8		-6.5		-3.1	0
640.0	642.0	C	48.7	119	2.6	342	292	6.5	6.9	-2.8		-6.9		-3.5	0
642.0	644.0	C	45.2	141	2.6	344	288	6.5	6.9	-1.0		-5.1		-4.4	0
644.0	646.0	B	36.4	117	2.6	345	281	6.5	6.8	-1.6		-4.4		-2.7	0
646.0	648.0	B	36.8	121	2.6	345	283	6.5	6.8	-1.3		-4.4		-2.6	0
648.0	650.0	C	34.9	115	2.6	342	282	6.5	6.8	-1.6		-4.2		-2.4	0
669.0	671.0	B	8.0	66	2.5	338	265	6.6	6.9	-.4		-.8		.2	0
672.0	674.0	B	5.6	53	2.6	339	271	6.6	6.9	-.2		-.4		.5	0
681.0	683.0	C	7.3	3	2.5	336	271	6.8	7.1	-.6		.1		.6	0
684.0	686.0	C	7.8	336	2.5	335	270	6.7	7.2	-.4		.5		.8	0
690.0	692.0	C	11.3	10	2.5	333	266	6.7	7.2	-.7		-.2		1.0	0
695.0	697.0	B	10.7	6	2.5	337	263	6.7	7.0	-.4		-.2		1.2	0
701.0	703.0	C	6.8	42	2.5	339	258	6.8	7.1	-1.0		-.6		-.2	0
704.0	706.0	B	9.8	3	2.5	336	260	6.8	7.1	-.8		-.2		.7	0
716.0	718.0	C	3.9	27	2.5	337	261	6.8	7.2	-.6		-.2		.1	0
723.0	725.0	B	7.9	14	2.5	337	261	6.8	7.1	-1.0		-.3		.2	0
731.0	733.0	C	6.7	360	2.4	333	258	6.8	7.0	-.4		-.1		.7	0
738.0	740.0	C	3.4	44	2.4	334	254	6.8	7.1	-.4		-.3		.1	0
744.0	746.0	C	8.5	69	2.4	338	249	6.8	7.2	-.4		-1.0		-.1	0
749.0	751.0	C	4.9	40	2.4	335	248	6.7	7.3	-.4		-.5		.2	0
756.0	758.0	C	6.4	29	2.4	338	248	6.8	7.1	-.9		-.6		-.1	0
763.0	765.0	C	7.0	69	2.4	335	249	6.7	7.0	-.4		-.4		-.2	0
769.0	771.0	C	8.5	36	2.4	337	245	6.7	7.1	-.4		-.4		-.3	0
784.0	786.0	A	6.1	49	2.3	336	245	6.7	7.1	-.7		-.7		-.2	0
820.0	822.0	B	6.8	10	2.2	336	249	6.7	7.0	-.4		-.4		-.2	0
828.0	830.0	C	8.7	24	2.2	332	255	6.7	7.1	-.4		-.6		.7	0
832.0	834.0	B	8.2	25	2.1	331	253	6.7	7.0	-1.0		-.6		.0	0
834.0	836.0	B	6.1	12	2.1	331	253	6.7	6.9	-.8		-.3		.1	0
874.0	878.0	C	6.4	21	1.9	332	247	6.7	7.0	-.7		-.5		.1	0
884.0	886.0	B	9.0	11	1.9	333	252	6.7	7.0	-.7		-.5		.5	0
888.0	890.0	C	5.7	20	1.9	330	256	6.7	7.0	-.6		-.3		.2	0
892.0	894.0	C	7.3	30	1.9	329	251	6.7	6.9	-.8		-.6		.0	0
903.0	905.0	A	5.7	319	1.9	333	245	6.8	7.0	-.1		.2		.8	0
938.0	940.0	B	6.3	41	1.9	327	250	6.7	7.0	-.8		-.6		-.2	0
946.0	948.0	A	6.7	33	1.7	329	250	6.7	7.0	-.6		-.6		.1	0
960.0	962.0	C	7.6	305	1.7	324	246	6.8	6.9	.0		.5		1.0	0
968.0	970.0	C	9.9	343	1.7	327	242	6.8	6.9	-.5		-.2		.9	0
974.0	976.0	C	6.0	346	1.6	326	239	6.8	6.9	-.6		-.2		.3	0
982.0	984.0	C	11.9	351	1.7	325	243	6.7	6.9	-1.4		-.4		.2	0
985.0	987.0	C	9.7	355	1.7	325	243	6.7	6.9	-.8		-.4		.5	0
990.0	992.0	C	13.8	338	1.6	324	240	6.7	7.0	-1.0		-.2		.9	0
998.0	1000.0	B	4.7	348	1.6	326	236	6.6	6.8	-.5		-.2		.2	0
1005.0	1006.0	C	6.7	4	1.5	320	234	6.7	6.8	.0		-.5		.8	0
1006.0	1008.0	0	5.4	63	1.5	315	236	6.7	6.8	-.1		-.6		.0	0
1010.0	1010.5	C	6.4	35	1.5	327	258	6.8	6.9	-1.0		-.5		-.3	0
1016.5	1017.5	B	13.3	41	1.6	326	239	6.7	6.9	-.4		-1.5		.3	0
1018.5	1020.0	C	.9	330	1.6	327	238	6.7	6.9	-.6		.0		-.3	0
1021.0	1021.5	C	2.0	31	1.6	327	238	6.6	6.9	-.1		-.2		.2	0

CORRELATION INTERVAL	CORR. GRADE	DIP ANG.	DIP AZ.	DRIFT ANG.	DRIFT AZ.	AZ. NO.1	DIA 13	DIA 24	DISPLACEMENTS					M	
									H12	H23	H13	H24	H14		
1024.5	1025.5	B	2.4	99	1.6	326	238	6.6	7.0	-.5		-.2		-.5	0
1031.5	1032.5	C	1.1	53	1.4	324	244	6.6	7.0	.2		-.1		.4	0
1032.5	1034.0	C	4.0	5	1.5	323	245	6.7	7.0	-.2		-.2		.4	0
1034.0	1035.1	B	7.6	345	1.5	323	246	6.7	7.0	-.4		-.1		.7	0
1036.0	1038.0	B	3.8	63	1.5	323	246	6.7	7.0	-.4		-.4		-.2	0
1038.0	1040.0	B	6.2	13	1.5	323	246	6.7	7.1	-.8		-.4		.0	0
1040.0	1042.0	B	1.5	27	1.5	323	247	6.8	7.1	-.6		-.1		-.3	0
1042.0	1043.5	B	4.9	45	1.4	323	247	6.7	7.0	-.4		-.5		.0	0
1046.5	1048.0	C	2.4	98	1.4	323	242	6.7	6.9	.0		-.2		.0	0
1048.0	1048.5	C	5.9	359	1.4	319	240	6.7	6.9	-.6		-.5		.2	0
1054.0	1056.0	C	1.1	337	1.4	320	237	6.8	6.9	-.3		.0		.0	0
1056.3	1058.0	C	2.8	331	1.4	321	237	6.7	6.9	-.4		.0		.1	0
1058.0	1059.0	C	4.4	3	1.4	322	237	6.7	7.0	-.8		-.3		-.2	0
1075.5	1076.5	C	5.2	38	1.4	322	230	6.7	6.9	-.6		-.6		-.3	0
1086.0	1088.0	C	3.9	345	1.4	318	229	6.7	7.0	-.2		-.2		.4	0
1090.0	1092.0	C	7.1	82	1.4	318	229	6.7	7.0	.3		-.7		.0	0
1105.5	1107.5	D	15.6	293	1.4	324	223	6.7	6.9	-1.8		.6		.2	0
1120.0	1120.5	C	7.4	295	1.3	325	192	6.6	6.9	-.2		-.3		.8	0
1132.5	1133.5	C	6.9	213	1.3	326	184	6.8	6.9	.1		.6		.6	0
1142.0	1142.7	B	3.6	12	1.2	322	170	6.6	6.9	-.1		-.5		-.2	0
1144.5	1146.5	C	8.2	320	1.2	323	167	6.7	6.9	-.5		-1.0		.0	0
1158.0	1160.0	C	.4	113	1.2	323	158	6.8	6.9	.1		-.1		.1	0
1160.5	1162.0	B	10.6	346	1.2	323	159	6.8	6.9	.0		-1.4		-.1	0
1162.5	1164.5	B	6.8	35	1.2	320	161	6.6	6.8	.2		-.6		-.4	0
1164.5	1165.5	B	10.1	270	1.2	319	161	6.6	6.7	-1.4		-.5		-.2	0
1166.0	1168.0	C	4.3	298	1.2	323	161	6.7	6.9	-.7		-.5		-.3	0
1174.0	1176.5	C	3.8	265	1.2	323	166	6.8	6.9	-.3		-.2		.2	0
1178.0	1179.5	B	9.0	17	1.1	322	161	6.8	6.9	-.2		-1.0		-.8	0
1185.0	1185.5	C	2.1	53	1.1	324	161	6.8	6.9	.2		-.2		-.4	0
1194.5	1195.5	C	5.9	98	1.2	319	89	6.8	6.9	-.4		-.4		.4	0
1197.0	1198.5	C	5.0	287	1.2	318	79	6.7	6.9	.4		-.4		.0	0
1199.5	1200.0	C	4.4	169	1.2	317	78	6.7	6.8	-.4		-.4		.0	0
1202.7	1204.5	B	4.4	213	1.2	317	75	6.6	6.8	.4		-.1		.3	0
1215.5	1216.1	C	2.7	106	1.1	318	62	6.8	7.0	-.3		.2		-.2	0
1218.0	1220.0	B	3.9	318	1.1	319	58	6.8	6.9	.4		-.1		-.2	0
1220.0	1222.0	B	3.5	296	1.1	319	53	6.8	6.9	.3		-.2		-.2	0
1222.0	1224.0	C	2.2	269	1.1	319	50	6.8	6.9	.3		-.2		.0	0
1224.0	1226.0	B	.6	311	1.1	321	47	6.7	6.9	.0		.0		.2	0
1226.0	1228.0	B	3.5	264	1.1	322	44	6.8	6.9	.0		-.3		-.4	0
1228.0	1230.0	B	9.8	181	1.1	320	38	6.8	7.0	-.7		-.4		-.1	0
1230.0	1232.0	C	3.6	64	1.1	319	33	6.8	6.9	.3		.4		.4	0
1232.0	1234.0	C	2.6	306	1.1	319	13	6.8	6.9	.7		.2		.3	0
1236.0	1237.5	B	4.3	44	1.1	318	8	6.8	6.9	.2		.5		.4	0
1246.0	1247.0	B	5.2	10	1.1	315	9	6.8	7.0	.7		.7		.6	0
1247.0	1249.0	B	4.4	13	1.0	316	12	6.8	7.0	.6		.6		.5	0
1267.7	1267.9	C	1.6	287	1.1	317	10	6.9	6.9	.5		.1		.2	0
1268.0	1268.9	C	2.9	131	1.1	317	10	6.9	6.9	.3		-.1		.5	0
1270.0	1272.0	B	.9	84	1.1	316	10	6.7	6.9	.0		.1		.0	0
1272.0	1273.5	B	2.9	224	1.0	320	9	6.7	6.9	.2		-.2		-.1	0
1274.0	1276.0	B	2.8	22	1.0	324	8	6.7	6.9	.2		.4		.2	0
1276.0	1278.0	B	4.3	70	1.0	326	4	6.8	6.9	.2		.3		.6	0
1278.0	1280.0	B	6.6	78	1.0	326	3	6.7	6.9	-.3		.3		.4	0
1280.0	1282.0	B	2.2	141	1.0	326	1	6.7	6.9	.0		-.1		.1	0
1282.0	1284.0	B	2.9	148	1.0	323	356	6.8	6.9	-.2		-.2		-.1	0
1284.0	1286.0	B	3.4	162	1.0	321	351	6.8	6.9	-.1		-.3		-.1	0

CORRELATION INTERVAL	CORR. GRADE	DIP ANG.	DIP AZ.	DRFT ANG.	DRFT AZ.	AZ. NO.1	DIA 13	DIA 24	DISPLACEMENTS					M
									H12	H23	H13	H24	H14	
1286.0	1288.0	C	1.8	153	1.0	320	349	6.8	6.9	.1	-.1		.1	0
1291.0	1291.3	C	5.2	136	1.0	318	351	6.7	7.0	.3	-.4		.6	0
1298.0	1300.0	B	9.6	51	.9	318	348	6.7	7.0	-.2	.6		.8	0
1300.0	1300.3	C	6.7	54	1.0	315	346	6.7	7.0	-.3	.4		.4	0
1303.3	1304.3	C	11.6	21	.9	316	344	6.7	7.0	.2	1.2		1.0	0
1309.0	1310.0	B	13.7	54	.9	314	338	6.7	6.9	-.4	.5		1.2	0
1314.5	1315.3	B	6.0	336	.9	311	333	6.7	7.0	.9	.8		.9	0
1345.5	1346.3	C	11.8	26	.8	341	231	6.7	6.9	-.9	-1.3		-.2	0
1346.3	1346.0	C	10.9	17	.9	342	224	6.7	6.9	-1.4	-1.2		-.7	0
1348.0	1349.0	C	9.8	10	1.0	332	215	6.7	6.9	-1.2	-1.1		-.6	0
1350.0	1351.3	C	11.3	52	1.0	321	201	6.7	6.9	-.3	-1.2		-.9	0
1352.0	1353.5	C	2.8	77	1.0	313	194	6.6	6.9	-.4	-.2		-.6	0
1366.0	1366.5	B	13.2	29	1.0	320	184	6.7	6.9	-.4	-1.5		-1.0	0
1377.0	1378.0	B	11.0	18	1.0	313	126	6.6	6.9	.3	-.5		-1.0	0
1379.5	1380.3	C	8.1	40	1.0	317	123	6.6	6.8	.6	.0		-.4	0
1385.0	1385.5	C	16.5	50	1.0	311	109	6.7	6.9	1.4	.9		-.4	0
1386.5	1388.0	B	5.4	18	1.0	311	107	6.6	6.9	.7	-.1		.0	0
1388.0	1390.0	C	11.1	40	1.0	312	107	6.7	6.9	.8	.4		-.5	0
1390.0	1392.0	C	5.3	11	1.0	311	101	6.7	6.9	.3	-.1		-.4	0
1392.0	1394.0	C	10.4	41	1.0	309	96	6.7	6.9	.9	.6		-.2	0
1394.0	1395.5	C	7.9	17	1.0	308	95	6.7	6.9	.8	.1		-.2	0
1396.0	1398.0	C	10.2	41	1.0	305	89	6.7	6.9	1.0	.7		.0	0
1398.0	1400.0	C	12.3	24	1.0	306	85	6.6	6.9	1.1	.6		-.3	0
1402.0	1404.5	B	7.2	49	1.0	298	71	6.6	6.8	1.0	.7		.6	0
1421.0	1421.3	C	4.5	6	.9	324	359	6.6	6.9	1.7	.6		1.7	0
1428.0	1429.3	C	21.0	69	.9	322	333	6.8	6.9	-1.7	-.2		.9	0
1431.0	1432.5	C	10.7	39	.9	325	317	6.9	6.9	-.4	.5		.9	0
1447.7	1447.9	D	19.4	1	.8	334	226	6.7	6.8	-2.0	-1.7		-.2	0
1451.7	1452.2	C	10.0	634	.8	330	192	6.6	6.8	-1.0	-1.0		-.2	0
1458.5	1460.0	C	8.7	69	.9	313	107	6.7	6.8	1.5	.7		-.2	0
1460.0	1462.0	C	11.0	61	1.0	312	107	6.7	6.8	-1.2	.6		.2	0
1462.0	1464.0	B	19.5	53	1.0	311	107	6.7	6.8	-1.7	.3		-.3	0
1466.0	1466.0	H	13.0	45	1.0	311	104	6.7	6.8	.6	.7		-.8	0
1482.5	1483.0	C	33.4	348	1.0	306	71	6.6	6.8	5.7	.5		1.1	0
1508.3	1508.7	B	9.1	44	1.1	309	5	6.7	6.9	.3	.9		.9	0
1514.0	1514.5	B	17.8	163	1.0	309	358	6.7	6.8	.0	-2.0		.5	0
1538.0	1540.5	C	20.8	137	1.0	312	0	6.8	6.9	-1.5	-1.8		.2	0
1543.5	1544.5	C	23.4	48	1.0	311	3	6.7	6.8	-.2	2.1		1.8	0
1557.9	1558.3	C	17.3	62	1.0	310	5	6.7	6.9	-.5	1.2		1.2	0
1560.0	1562.0	B	15.3	48	1.0	311	4	6.7	6.9	.1	1.4		1.3	0
1563.5	1564.5	C	24.8	4	1.0	312	4	6.7	6.9	.5	3.2		.4	0
1593.8	1594.7	C	28.0	71	1.0	309	346	6.8	7.0	-2.7	.4		.9	0
1604.0	1606.0	C	3.2	19	1.0	323	341	6.6	6.9	1.9	.4		2.1	0
1610.0	1612.0	C	12.1	68	1.0	315	321	6.5	6.9	-.5	-.3		.9	0
1618.0	1620.0	B	29.0	30	1.0	309	289	6.7	6.9	-1.6	-.6		2.2	0
1622.0	1624.0	A	26.0	48	1.0	308	283	6.8	6.9	-1.3	-1.8		1.5	0
1624.0	1626.0	B	25.7	53	1.0	309	278	6.8	6.9	-1.5	-2.2		.9	0
1628.0	1630.0	A	25.3	26	1.0	307	274	6.8	6.9	-2.2	-1.1		.9	0
1632.0	1634.0	A	19.2	35	1.0	305	268	6.7	6.9	-1.6	-1.3		.4	0
1636.0	1638.0	A	21.7	37	1.1	304	265	6.7	6.8	-.9	-1.7		1.2	0
1640.0	1642.0	B	28.9	36	1.1	303	262	6.7	6.9	-1.8	-2.5		1.0	0
1643.0	1644.0	A	13.6	13	1.1	307	258	6.7	6.9	-1.5	-.6		.1	0
1645.0	1646.0	C	10.3	17	1.1	310	259	6.7	6.9	-.7	-.5		.5	0
1654.0	1656.0	B	25.8	36	1.1	307	244	6.7	6.9	-1.7	-2.8		.0	0
1658.0	1660.0	B	12.0	38	1.1	304	238	6.6	6.8	-1.0	-1.3		-.4	0

CORRELATION INTERVAL	CURR. GRADE	DIP ANG.	DIP AZ.	DRFT ANG.	DRFT AZ.	AZ. NO.1	DIA 13	DIA 24	DISPLACEMENTS					M
									H12	H23	H15	H24	H14	
1662.0	1664.0	A	18.6	35	1.1	303	230	6.6	6.7	-1.1	-2.1		-.4	0
1666.0	1668.0	A	22.3	43	1.1	308	231	6.7	6.8	-1.9	-2.7		-1.4	0
1669.0	1670.0	A	21.8	24	1.1	309	229	6.7	6.8	-1.6	-2.4		-.3	0
1672.0	1674.0	B	21.2	65	1.1	310	229	6.8	6.8	-2.4	-2.5		-3.0	0
1678.0	1680.0	B	12.5	81	1.1	308	222	6.5	6.6	-.3	-1.1		-1.1	0
1680.0	1682.0	B	19.5	31	1.1	315	218	6.5	6.6	-.7	-2.3		-.3	0
1686.0	1688.0	A	20.1	46	1.1	317	220	6.5	6.8	-1.0	-2.4		-1.1	0
1690.0	1692.0	B	11.8	0	1.1	318	220	6.5	6.7	-1.5	-1.3		-.9	0
1695.0	1696.0	C	18.7	33	1.1	321	223	6.5	6.6	-1.3	-2.2		-.6	0
1699.0	1700.0	C	15.7	55	1.1	315	221	6.5	6.7	.5	-1.8		.2	0
1700.0	1702.0	C	13.4	342	1.1	315	221	6.5	6.7	-.3	-.8		1.2	0
1702.0	1704.0	C	13.7	39	1.0	317	222	6.5	6.7	-1.3	-1.6		-1.1	0
1706.0	1708.0	A	14.6	41	1.0	317	223	6.5	6.7	-1.0	-1.7		-.8	0
1714.0	1716.0	B	12.7	85	1.0	322	223	6.5	6.7	-.2	-1.1		-1.1	0
1721.0	1722.0	B	8.4	83	1.0	327	216	6.5	6.7	.1	-.7		-.5	0
1725.0	1726.0	D	19.5	355	1.1	324	208	6.5	6.6	-1.3	-2.0		.1	0
1729.0	1730.0	B	3.9	342	1.1	322	202	6.5	6.6	-.6	-.4		-.2	0
1732.0	1733.0	B	8.1	93	1.2	323	197	6.5	6.6	-.3	-.3		-1.1	0
1735.0	1736.0	B	10.3	36	1.2	323	196	6.5	6.6	-.2	-1.2		-.5	0
1736.0	1738.0	B	12.7	32	1.2	323	196	6.5	6.6	.0	-1.5		-.3	0
1740.0	1742.0	C	12.2	63	1.2	324	193	6.5	6.7	.5	-1.0		-.5	0
1746.0	1748.0	B	18.5	59	1.2	323	197	6.5	6.8	-1.0	-1.7		-2.4	0
1752.0	1754.0	B	25.8	310	1.2	322	198	6.6	6.8	-1.7	-1.3		1.5	0
1758.0	1760.0	B	4.4	2	1.1	324	193	6.7	6.9	-.5	-.6		-.3	0
1760.0	1762.0	A	16.7	16	1.1	325	188	6.7	6.9	-.8	-2.1		-1.0	0
1767.0	1768.0	A	8.1	12	1.0	346	168	6.8	6.9	-.1	-1.0		-.5	0
1770.0	1772.0	A	6.9	264	1.0	345	161	6.7	6.8	.4	-.3		1.2	0
1775.0	1776.0	C	59.7	274	1.1	338	138	6.7	6.8	-4.3	-4.2		-.4	0
1780.0	1782.0	B	7.0	50	1.2	331	129	6.7	6.9	.5	-.2		-.4	0
1784.0	1786.0	A	22.6	31	1.3	328	109	6.7	6.9	2.1	-.5		-.8	0
1789.0	1790.0	C	11.7	36	1.3	330	101	6.8	6.9	.9	-.4		-.6	0
1791.0	1792.0	B	17.4	87	1.3	333	97	6.8	6.9	2.2	2.0		1.7	0
1796.0	1797.0	A	17.3	73	1.3	323	82	6.8	6.9	1.4	2.0		.9	0
1799.0	1800.0	C	10.6	101	1.3	326	81	6.6	7.0	.2	1.1		.5	0
1801.0	1802.0	D	8.2	22	1.3	328	71	6.7	6.9	.9	.6		.0	0
1804.0	1805.0	A	8.4	30	1.3	319	63	6.7	6.9	.9	.6		.2	0
1807.0	1808.0	A	8.5	34	1.3	327	60	6.7	7.0	1.1	.9		.5	0
1809.0	1810.0	A	13.1	30	1.3	330	57	6.7	7.0	1.2	1.4		.3	0
1811.0	1812.0	A	12.8	33	1.3	332	49	6.7	7.1	1.1	1.5		.5	0
1816.0	1818.0	A	8.6	56	1.3	329	31	6.7	6.9	.7	1.0		1.0	0
1819.0	1820.0	A	14.9	62	1.3	328	31	6.7	6.9	.5	1.6		1.3	0
1821.0	1822.0	A	17.3	53	1.3	328	30	6.7	6.9	.6	2.0		1.3	0
1824.0	1826.0	A	10.9	16	1.3	328	11	6.7	6.9	1.0	1.4		1.0	0
1826.0	1828.0	A	14.2	19	1.3	328	9	6.7	6.9	.9	1.8		1.1	0
1829.0	1830.0	B	16.6	18	1.3	334	4	6.7	6.9	.6	2.1		1.0	0
1835.0	1836.0	A	11.8	38	1.3	331	340	6.8	6.9	.6	.9		1.8	0
1837.0	1838.0	A	10.4	55	1.3	335	327	6.8	7.0	-.1	.2		1.2	0
1839.0	1840.0	A	13.5	13	1.3	336	314	6.8	7.0	.0	1.0		1.5	0
1842.0	1843.0	A	9.7	20	1.2	333	294	6.8	7.0	-.5	.2		.8	0
1844.0	1846.0	A	19.8	39	1.3	324	274	6.8	7.0	-1.3	-1.3		.9	0
1847.0	1848.0	A	8.1	43	1.3	323	267	6.7	6.9	-.5	-.6		.3	0
1851.0	1852.0	C	13.7	25	1.3	322	259	6.7	6.9	-.8	-.9		.7	0
1857.0	1858.0	C	10.7	13	1.3	326	252	6.7	7.0	-1.7	-.6		-.4	0
1865.0	1866.0	C	21.9	28	1.3	328	232	6.7	7.0	-1.3	-2.5		.0	0
1873.0	1874.0	D	2.6	271	1.4	340	204	6.6	6.9	-1.7	.0		-1.3	0

CORRELATION INTERVAL	CORR. GRADE	DIP ANG.	DIP AZ.	DRIFT ANG.	DRIFT AZ.	AZ. NO.	DIA 15	DIA 24	DISPLACEMENTS						
									H12	H23	H13	H24	H14	M	
1880.0	1882.0	C	19.8	42	1.3	329	176	6.6	6.8	1.2	-1.8			-.5	0
1890.0	1892.0	B	18.9	281	1.3	335	166	6.8	6.9	-1.9	-1.1			.3	0
1894.0	1895.0	C	32.9	350	1.3	333	153	6.8	6.9	-3.6	-4.4			-4.9	0
1902.0	1904.0	C	24.8	8	1.3	333	105	6.7	7.1	2.3	-.5			-1.1	0
1916.0	1911.0	B	53.8	229	1.4	338	103	6.8	6.5	-2.5	-2.7			.9	0
1917.0	1918.0	C	15.5	320	1.4	341	100	6.6	6.9	-.7	-1.5			-2.1	0
1928.0	1929.0	C	11.3	324	1.3	337	105	6.5	6.8	-.1	-1.1			-1.1	0
1931.0	1932.0	C	20.1	321	1.3	337	100	6.5	6.5	.0	-1.9			-1.7	0
1952.0	1954.0	C	47.4	259	1.3	341	53	6.7	6.8	-2.9	-6.5			-6.3	0
1966.0	1968.0	C	50.4	242	1.2	349	61	6.6	6.7	-3.6	-7.9			-3.9	0
1974.0	1976.0	B	19.4	351	1.2	346	69	6.6	6.8	1.2	.5			-1.3	0
1980.0	1982.0	A	7.6	307	1.2	350	60	6.7	7.0	.7	-.3			-.3	0
1983.0	1984.0	A	6.2	315	1.2	353	51	6.6	7.2	.8	.0			-.1	0
1985.0	1986.0	A	9.3	343	1.1	360	51	6.6	7.2	1.1	.5			-.1	0
1987.0	1988.0	A	9.6	308	1.1	350	28	6.7	7.3	1.0	.3			-.3	0
1998.0	1999.0	C	15.9	301	1.1	351	353	6.7	7.1	2.5	1.3			.9	0
2002.0	2003.0	A	15.4	329	1.1	350	342	6.6	6.9	1.1	1.9			.7	0
2006.0	2008.0	A	16.7	315	1.1	351	357	6.6	6.9	2.1	1.6			.7	0
2010.0	2012.0	A	8.4	353	1.0	350	3	6.8	6.7	.9	1.1			.7	0
2015.0	2016.0	A	6.5	313	1.0	355	4	6.6	6.7	1.3	.6			.7	0
2019.0	2020.0	A	14.0	331	1.0	359	4	6.6	6.6	1.3	1.5			.4	0
2022.0	2023.0	A	16.1	343	1.0	354	343	6.8	6.6	1.4	2.1			1.4	0
2026.0	2027.0	A	15.6	330	.9	347	340	6.8	6.6	1.3	2.0			1.0	0
2029.0	2030.0	B	14.3	353	.9	351	359	6.6	6.8	1.2	1.8			1.0	0
2031.0	2032.0	A	15.2	3	.9	352	5	6.6	6.8	1.1	1.9			1.0	0
2033.0	2034.0	A	7.7	360	.9	354	5	6.6	6.8	.8	1.0			.7	0
2035.0	2036.0	A	11.8	332	.9	356	5	6.8	6.8	1.6	1.3			.8	0
2039.0	2040.0	B	8.7	332	.9	357	360	6.6	6.9	.9	1.0			.4	0
2043.0	2044.0	B	6.6	34	.9	354	353	6.7	6.8	1.4	1.1			.6	0
2047.0	2048.0	B	11.0	355	.9	352	3	6.9	6.8	1.3	1.5			1.1	0
2049.0	2050.0	B	14.4	330	.9	354	6	6.9	6.8	1.6	1.6			.5	0
2051.0	2052.0	A	7.2	31	.9	357	39	6.8	6.8	1.1	.9			1.4	0
2057.0	2058.0	A	10.6	37	.8	355	358	6.9	6.8	.9	1.1			1.7	0
2058.0	2062.0	A	4.7	34	.8	2	351	6.8	6.8	1.1	.5			1.5	0
2063.0	2064.0	A	17.8	355	.8	359	348	6.6	6.8	1.1	2.2			1.4	0
2067.0	2068.0	A	10.8	11	.8	359	353	6.6	6.8	.7	1.3			1.1	0
2068.0	2069.0	A	18.1	349	.8	360	354	6.8	6.8	1.2	2.3			1.0	0
2073.0	2074.0	A	14.9	16	.8	3	357	6.8	6.8	.9	1.8			1.5	0
2077.0	2078.0	A	17.5	293	.8	3	1	6.7	6.8	2.3	.9			.3	0
2084.0	2085.0	C	7.5	342	.9	3	344	6.8	6.7	.9	1.0			.9	0
2088.0	2089.0	C	9.9	319	.9	4	341	6.8	7.0	1.9	1.2			1.5	0
2092.0	2093.0	A	12.8	315	.9	4	340	6.8	6.9	1.6	1.5			1.0	0
2096.0	2097.0	C	12.7	33	.9	6	339	6.7	6.9	.0	1.0			1.3	0
2101.0	2102.0	C	12.5	353	.9	2	346	6.8	6.9	.9	1.6			1.1	0
2103.0	2104.0	A	15.7	3	.8	2	346	6.7	6.7	.7	1.9			1.3	0
2106.0	2108.0	A	17.3	355	.8	1	339	6.7	6.7	.7	2.1			1.3	0
2111.0	2112.0	B	23.3	5	.8	1	337	6.8	6.7	.9	2.7			2.3	0
2113.0	2114.0	B	11.0	345	.8	1	334	6.9	6.6	1.4	1.4			1.7	0
2115.0	2116.0	B	12.8	78	.8	2	334	6.9	6.6	.3	-.3			1.8	0
2119.8	2120.0	C	10.5	23	.8	4	332	7.0	6.6	.1	.9			1.1	0
2122.0	2123.0	B	12.0	29	.8	4	328	7.0	6.7	.1	.6			1.4	0
2127.0	2128.0	A	17.6	3	.8	6	328	7.0	6.7	.6	1.9			1.9	0
2131.0	2132.0	B	11.9	353	.8	6	326	7.0	6.8	.4	1.4			1.1	0
2135.0	2136.0	B	16.0	20	.8	8	324	7.0	6.8	.2	1.2			1.9	0
2138.0	2139.0	A	16.5	25	.7	9	321	7.1	6.9	.7	1.0			2.6	0

CORRELATION INTERVAL	CORR. GRADE	DIP ANG.	DIP AZ.	DRIFT ANG.	DRIFT AZ.	AZ. NO.	DIA 13	DIA 24	DISPLACEMENTS					M	
									H12	H23	H13	H24	H14		
2144.0	2145.0	C	13.9	291	.7	7	321	7.1	7.1	1.4		1.6		.6	0
2149.0	2150.0	C	8.5	356	.7	9	319	7.0	7.0	.0		.9		.7	0
2154.0	2154.3	C	16.3	222	.7	171	324	7.0	6.8	1.1		-.5		-.9	0
2159.8	2160.3	B	50.0	355	.7	9	305	7.1	7.0	-.3		2.7		2.9	0
2163.0	2164.0	B	10.9	64	.7	11	311	7.0	7.0	-.6		-.5		.7	0
2164.0	2165.0	B	18.0	32	.7	9	311	6.9	6.9	-.8		.4		1.5	0
2167.0	2168.0	A	16.0	19	.7	14	324	7.0	6.9	-.5		1.2		1.2	0
2168.0	2169.0	A	13.1	38	.7	14	324	7.0	6.9	-.2		.5		1.4	0
2171.0	2172.0	B	13.7	30	.7	12	326	7.0	6.9	-.3		.6		1.3	0
2173.0	2174.0	A	12.4	38	.7	28	329	7.1	6.9	.0		.6		1.5	0
2177.0	2178.0	A	14.4	28	.7	31	334	6.9	6.9	-.1		1.1		1.4	0
2180.0	2181.0	C	11.3	359	.8	27	332	6.9	7.0	1.3		1.3		2.0	0
2185.0	2186.0	B	19.8	46	.8	30	340	6.9	7.1	-.6		1.1		1.8	0
2190.0	2191.0	A	25.6	18	.7	33	340	6.7	6.8	-1.1		2.6		1.0	0
2194.0	2194.5	B	5.4	20	.7	35	336	6.7	6.7	-.5		.5		.0	0
2196.0	2197.0	B	8.3	168	.7	37	332	6.7	7.0	-.1		-.9		-.3	0
2199.0	2200.0	C	11.5	37	.7	41	331	6.9	7.1	-.5		.6		.9	0
2201.0	2202.0	D	14.1	106	.7	35	321	6.9	7.1	-.7		-1.4		.4	0
2204.0	2205.0	B	19.5	126	.7	46	329	7.2	7.1	-1.9		-2.3		-.8	0
2208.0	2210.0	A	13.4	56	.7	49	350	6.9	7.0	-.4		.7		1.2	0
2211.0	2212.0	B	14.2	302	.7	51	353	6.7	6.9	.9		1.1		-.4	0
2214.0	2215.0	A	8.9	331	.7	53	357	6.7	6.9	.6		1.0		.2	0
2218.0	2219.0	C	17.9	25	.7	56	0	6.6	6.9	.0		2.0		1.0	0

A. C. ... Company

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THE FOLLOWING PARAMETERS APPLY TO THE LOG FROM 578.0 FEET TO 2219.0

MAGNETIC DECLINATION IS 20.0 DEGREES.

THE 1 ON 2 CORRELATIONS HAVE BEEN CORRECTED .0 INCHES.

THE 1 ON 3 CORRELATIONS HAVE BEEN CORRECTED .0 INCHES.

THE 1 ON 4 CORRELATIONS HAVE BEEN CORRECTED .2 INCHES.

THE 2 ON 3 CORRELATIONS HAVE BEEN CORRECTED .0 INCHES.

THE 2 ON 4 CORRELATIONS HAVE BEEN CORRECTED .2 INCHES.

DRIFT AZIMUTH AND AZIMUTH OF NO. 1 ARM HAVE BEEN CORRECTED TO TRUE NORTH IN THIS PRESENTATION.

WATER LOGGING COMPANY

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