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DEPT OF GEOLOGY
& MINERAL INDUST

DIP LOG CALCULATIONS

COMPANY REICHHOLD ENERGY CORPORATION
WELL CROWN ZELLERBACH 22-6 RD. No.2
FIELD MIST NEHALEM BASIN
COUNTY COLUMBIA STATE OREGON

WELEX

A **Halliburton** Company

CORRELATION INTERVAL	CORR. GRADE	DIP ANG.	DIP AZ.	DRFT ANG.	DRFT AZ.	AZ. NO.1	DIA 13	DIA 24	DISPLACEMENTS					
									H12	H23	H13	H24	H14	M
466.0	468.0	H	12.0	293	2.4	190	353	6.1	6.6	.9	.4	.4	.4	0
478.0	480.0	H	44.0	351	2.3	151	350	6.1	6.3	2.3	5.5	2.5	0	0
487.0	489.0	C	49.1	313	2.8	141	350	6.1	6.3	3.6	5.1	.4	0	0
493.0	495.0	C	47.6	126	3.1	126	338	6.1	6.4	-4.7	-6.3	.5	0	0
508.0	510.0	H	42.1	129	4.3	117	335	6.1	6.4	-4.2	-5.7	-1.2	0	0
522.0	524.0	D	23.3	303	5.1	105	321	6.1	6.4	1.3	2.0	.8	0	0
586.0	588.0	C	28.3	127	8.4	78	299	6.1	6.5	-2.8	-4.2	-2.7	0	0
596.0	598.0	C	34.2	120	9.3	76	294	6.1	6.4	-3.6	-5.4	-3.5	0	0
618.0	620.0	C	35.6	143	10.8	69	246	6.1	6.4	1.1	-2.2	-3.7	0	0
625.0	627.0	C	37.2	148	10.7	71	246	6.1	6.2	1.4	-1.9	-3.6	0	0
643.0	646.0	H	23.8	141	10.6	59	214	6.1	6.2	1.4	-.2	-1.8	0	0
648.0	650.0	C	11.9	272	10.6	58	210	6.1	6.3	.0	-.4	.6	0	0
674.0	676.0	H	6.0	12	10.4	49	206	6.2	6.4	-.5	-1.7	-.8	0	0
684.0	686.0	C	8.6	344	10.3	46	192	6.2	6.6	-1.1	-1.8	-1.3	0	0
699.0	701.0	H	6.5	347	10.3	36	170	6.2	6.4	.0	-1.5	-.8	0	0
708.0	711.0	D	17.1	253	10.0	38	170	6.2	6.5	-1.4	-.5	-.3	0	0
728.0	730.0	H	4.6	71	9.6	31	166	6.2	6.4	.1	-.8	-1.2	0	0
744.0	746.0	C	3.5	290	9.3	35	171	6.2	6.5	.2	-.9	-.2	0	0
750.0	752.0	C	15.8	116	9.1	352	171	6.2	6.5	1.0	.0	-.5	0	0
754.0	756.0	C	7.9	105	8.9	19	171	6.2	6.4	.4	-.5	-.9	0	0
768.0	770.0	C	2.7	324	8.7	19	172	6.2	6.4	-.1	-1.1	-.4	0	0
786.0	788.0	H	7.8	310	8.8	12	181	6.2	6.4	-1.4	-1.5	-.9	0	0
788.0	790.0	A	4.2	303	8.9	12	181	6.2	6.4	-.8	-1.2	-.6	0	0
812.0	814.0	C	15.7	305	9.1	360	210	6.2	6.4	-1.6	-1.0	.8	0	0
830.0	832.0	D	3.2	20	9.2	357	199	6.3	6.4	-1.4	-1.3	-1.0	0	0
840.0	842.0	C	6.6	293	9.5	357	226	6.3	6.4	-1.2	-.4	.3	0	0
878.0	880.0	C	1.6	22	10.0	355	229	6.3	6.4	-1.2	-.8	.6	0	0
884.0	886.0	H	3.5	301	9.9	358	217	6.2	6.3	-1.3	-.9	.0	0	0
892.0	894.0	H	4.8	315	10.0	356	202	6.2	6.4	-1.3	-1.2	.0	0	0
912.0	914.0	H	5.9	313	10.4	357	181	6.3	6.4	-1.3	-1.2	.0	0	0
948.0	950.0	C	16.0	32	11.7	1	181	6.3	6.3	-.4	-3.0	-1.4	0	0
956.0	958.0	D	2.5	337	12.0	360	180	6.3	6.3	-.8	-1.6	-.7	0	0
969.0	971.0	D	13.0	158	12.2	3	180	6.2	6.2	.8	.0	.2	0	0
978.0	980.0	C	7.0	275	12.2	5	181	6.2	6.2	-1.1	-1.4	-.4	0	0
986.0	988.0	H	4.6	354	12.3	359	181	6.3	6.2	-.8	-1.9	-.7	0	0
995.0	997.0	H	6.6	47	12.2	2	180	6.3	6.2	-.7	-1.9	-1.3	0	0
1008.0	1010.0	C	4.1	21	12.5	3	178	6.2	6.2	-.9	-1.8	-1.2	0	0
1014.0	1016.0	H	11.2	318	13.0	3	182	6.2	6.3	-1.5	-2.4	-.6	0	0
1042.0	1044.0	H	6.1	325	13.3	4	211	6.2	6.2	-1.3	-1.6	.0	0	0
1044.0	1046.0	C	9.7	308	13.3	360	217	6.1	6.2	-1.6	-1.2	.4	0	0
1046.0	1048.0	H	9.0	306	13.4	358	215	6.1	6.1	-1.5	-1.2	.4	0	0
1059.5	1060.0	C	10.6	322	13.5	1	214	6.2	6.3	-2.5	-1.7	-.5	0	0
1060.7	1061.0	C	8.6	63	13.6	359	214	6.2	6.3	-2.2	-2.1	-1.8	0	0
1063.5	1063.7	D	7.4	26	13.6	359	214	6.2	6.3	-2.1	-2.1	-1.1	0	0
1067.0	1068.0	C	2.2	23	13.7	358	212	6.2	6.2	-1.4	-1.5	-.5	0	0
1068.3	1070.0	H	8.3	340	13.7	358	211	6.2	6.2	-2.0	-1.9	-.4	0	0
1070.0	1071.3	H	2.2	276	13.7	359	210	6.2	6.2	-1.5	-1.2	-.5	0	0
1079.0	1080.3	H	9.2	359	13.8	0	197	6.2	6.2	-1.4	-2.5	-.6	0	0
1080.3	1081.5	H	7.9	291	13.9	0	189	6.2	6.2	-1.6	-1.7	-.5	0	0
1087.0	1089.0	C	8.5	224	14.0	0	184	6.2	6.2	-.4	-.8	.3	0	0
1103.0	1103.5	C	4.2	338	14.2	2	182	6.2	6.2	-.5	-2.0	-.3	0	0
1120.0	1121.3	D	22.4	177	14.3	9	182	6.3	6.2	-.3	-.9	-.7	0	0
1123.0	1124.3	C	17.4	15	14.3	9	182	6.2	6.2	-.1	-3.8	-.8	0	0
1130.0	1131.3	C	8.1	195	14.4	7	186	6.2	6.2	.0	-.7	.1	0	0
1135.3	1136.2	C	15.2	85	14.5	7	190	6.2	6.2	.6	-2.1	-1.0	0	0

CORRELATION INTERVAL	CORR. GRADE	DIP ANG.	DIP AZ.	DRFT ANG.	DRFT AZ.	AZ. NO.1	DIA 13	DIA 24	DISPLACEMENTS				
									H12	H23	H13	H24	H14
1137.0	1137.3	C	5.3	60	14.5	5	190	6.2	6.2	-2.0	-2.0	-2.3	0
1147.3	1147.9	B	8.7	258	14.6	8	192	6.1	6.2	-1.8	-1.2	-.8	0
1156.0	1158.0	C	9.1	329	14.9	6	195	6.2	6.2	-2.3	-2.4	-1.3	0
1158.0	1158.5	B	13.7	323	14.9	3	194	6.2	6.2	-2.3	-2.7	-.7	0
1159.0	1160.3	C	7.5	352	15.0	7	194	6.2	6.2	-1.0	-2.5	-.5	0
1163.0	1164.1	C	5.9	338	15.2	10	199	6.2	6.2	-1.3	-2.2	-.6	0
1166.5	1167.3	C	12.9	281	15.4	6	201	6.1	6.2	-2.2	-1.4	-.3	0
1170.0	1171.5	B	2.2	259	15.5	5	201	6.1	6.2	-1.4	-1.5	-.7	0
1175.3	1176.5	B	7.0	22	15.7	6	200	6.1	6.2	-1.1	-2.5	-.7	0
1176.5	1178.5	B	7.9	331	15.7	7	200	6.1	6.2	-2.0	-2.3	-.9	0
1178.5	1180.3	B	5.3	348	15.8	4	200	6.1	6.2	-1.9	-2.2	-1.1	0
1180.3	1182.0	B	8.4	345	15.8	2	200	6.1	6.2	-2.4	-2.5	-1.3	0
1182.0	1184.0	B	11.3	317	15.9	4	200	6.1	6.2	-2.9	-2.3	-1.2	0
1184.0	1186.0	C	1.5	145	15.9	6	201	6.2	6.2	-1.1	-1.6	-.8	0
1186.0	1188.0	C	3.6	96	15.9	5	202	6.2	6.2	-1.1	-1.8	-1.0	0
1188.5	1189.5	C	11.3	285	16.0	2	202	6.2	6.2	-1.7	-1.5	.2	0
1192.0	1194.0	C	2.2	39	16.0	0	202	6.2	6.2	-1.7	-1.4	-1.1	0
1194.0	1196.0	C	7.4	307	16.1	0	202	6.2	6.2	-2.0	-1.9	-.5	0
1196.0	1198.3	C	8.3	304	16.1	0	202	6.2	6.2	-1.8	-1.9	-.2	0
1199.5	1199.9	C	10.0	320	16.1	1	201	6.2	6.2	-3.1	-2.3	-1.4	0
1202.0	1204.0	B	9.8	353	16.2	1	201	6.3	6.3	-2.1	-2.8	-.9	0
1214.0	1215.0	B	8.7	357	16.3	5	204	6.3	6.3	-2.3	-2.7	-1.2	0
1216.5	1217.3	B	5.0	320	16.3	7	214	6.3	6.2	-2.1	-1.8	-.7	0
1219.5	1220.3	B	9.1	333	16.3	6	222	6.2	6.2	-2.1	-1.9	.0	0
1223.0	1224.5	B	.9	326	16.3	2	224	6.2	6.2	-2.0	-1.4	-.7	0
1236.3	1236.7	B	18.9	90	16.6	359	217	6.2	6.3	-1.6	-2.5	-2.4	0
1238.0	1240.0	C	7.8	339	16.7	4	216	6.2	6.3	-1.0	-2.1	-.8	0
1240.0	1242.3	B	7.5	37	16.8	4	216	6.2	6.3	-1.8	-2.5	-.9	0
1242.3	1243.3	B	7.3	15	16.9	360	215	6.2	6.3	-2.0	-2.3	-.4	0
1244.0	1246.0	B	14.4	127	17.0	357	212	6.2	6.4	-1.5	-1.8	-.9	0
1246.0	1247.5	B	9.7	318	17.1	3	210	6.2	6.4	-1.7	-2.1	-.3	0
1247.5	1249.3	B	6.2	345	17.1	1	211	6.2	6.3	-1.8	-2.2	-.3	0
1250.0	1251.3	C	11.7	209	17.2	358	211	6.2	6.3	-1.6	-.3	-.6	0
1252.3	1254.3	B	3.5	304	17.4	360	211	6.2	6.3	-.9	-1.7	.5	0
1254.5	1255.5	C	16.3	163	17.4	359	210	6.2	6.2	-.4	-.4	-.7	0
1256.0	1258.5	B	2.8	312	17.5	357	210	6.2	6.2	-1.5	-1.7	-.1	0
1258.5	1259.0	B	7.9	315	17.6	357	210	6.2	6.2	-1.7	-1.9	.3	0
1260.0	1262.0	C	11.3	311	17.6	2	210	6.2	6.2	-2.2	-2.0	.1	0
1265.5	1265.6	C	6.4	61	17.8	3	212	6.2	6.2	-1.8	-2.4	-1.2	0
1266.5	1267.3	B	7.1	270	17.9	2	212	6.2	6.3	-1.8	-1.3	-.1	0
1271.5	1272.5	C	6.3	334	18.0	359	213	6.2	6.3	-2.1	-2.1	-.3	0
1291.0	1292.0	B	2.2	63	18.0	355	200	6.2	6.2	-1.6	-2.0	-.9	0
1292.0	1294.0	B	4.4	290	18.0	355	201	6.2	6.2	-1.8	-1.8	-.4	0
1294.0	1296.3	B	4.2	349	18.0	0	201	6.2	6.2	-1.6	-2.3	-.6	0
1296.3	1298.0	B	8.4	336	18.0	360	202	6.2	6.2	-2.3	-2.6	-.8	0
1298.0	1299.3	B	5.5	334	18.0	358	202	6.2	6.2	-2.3	-2.3	-1.0	0
1299.3	1300.5	C	3.1	273	18.0	356	202	6.2	6.2	-1.3	-1.7	-.1	0
1302.0	1304.0	B	4.6	201	18.0	356	200	6.2	6.2	-1.7	-1.3	-.9	0
1304.0	1306.0	B	6.7	282	18.2	359	200	6.2	6.3	-2.2	-1.8	-.7	0
1306.0	1307.0	B	11.7	333	18.2	357	200	6.2	6.3	-2.0	-2.9	-.1	0
1328.2	1328.5	D	24.2	16	18.9	7	190	6.1	6.2	-2.6	-5.7	-2.8	0
1336.5	1338.1	C	31.4	12	19.2	8	195	6.1	6.2	-4.4	-7.4	-3.8	0
1340.0	1341.5	B	16.9	32	19.3	9	207	6.1	6.2	-2.3	-4.3	-1.8	0
1349.1	1349.7	B	22.1	240	19.4	0	209	6.1	6.2	-.9	.3	1.4	0
1419.0	1419.5	C	32.3	336	20.1	2	180	6.2	6.3	.0	-7.4	-2.7	2

CORRELATION INTERVAL	CORR. GRADE	DIP ANG.	DIP AZ.	DRFT ANG.	DRFT AZ.	AZ. NO.1	DIA 13	DIA 24	DISPLACEMENTS					
									H12	H23	H13	H24	H14	V
1434.3	1435.3	C	18.3	305	20.6	3	181	6.2	6.3	-2.8	-3.7		.0	4
1441.9	1443.0	B	9.1	105	21.2	2	186	6.2	6.2	-.8	-2.2		-1.7	0
1444.5	1445.3	B	28.6	69	21.2	357	186	6.2	6.2	-.6	-4.2		-3.7	0
1448.5	1449.5	B	7.9	334	21.1	1	180	6.2	6.2	-.8	-3.3		-.4	0
1449.5	1453.0	B	8.8	27	21.1	0	180	6.2	6.2	-1.6	-3.4		-2.1	0
1456.0	1456.5	B	23.8	116	21.1	358	180	6.1	6.3	1.1	-1.1		-1.3	0
1461.5	1462.5	B	10.4	92	21.2	360	178	6.2	6.3	-.9	-2.3		-2.2	0
1462.5	1464.0	B	3.1	237	21.2	358	175	6.2	6.3	-1.4	-2.2		-1.2	0
1490.0	1490.5	B	18.8	72	21.2	358	163	6.2	6.3	-.6	-2.4		-3.6	0
1507.0	1508.5	C	16.4	81	21.0	5	164	6.2	6.3	-.3	-2.0		-3.2	0
1510.0	1511.3	B	14.9	66	21.0	1	164	6.2	6.3	-.9	-2.6		-3.5	0
1516.5	1517.3	C	33.7	24	21.0	357	163	6.2	6.2	-2.6	-7.0		-7.1	0
1524.0	1526.5	B	31.7	302	21.0	358	157	6.2	6.3	-5.2	-6.3		-3.4	0
1530.0	1531.5	C	28.0	35	21.1	358	156	6.3	6.3	1.0	-4.6		-3.7	0
1541.0	1541.3	C	28.0	227	21.1	1	155	6.3	6.3	-4.0	-1.1		-2.0	0
1576.0	1577.5	B	2.9	359	20.6	358	170	6.3	6.2	-1.4	-2.7		-1.8	0
1579.0	1579.5	B	16.1	343	20.5	356	169	6.3	6.3	-2.8	-4.6		-2.9	0
1594.0	1595.5	B	44.3	209	20.0	3	162	6.3	6.3	-4.0	1.5		-1.1	0
1606.5	1607.3	C	22.0	196	19.6	2	164	6.2	6.2	-1.7	.0		-1.1	0
1608.0	1610.0	B	10.9	32	19.6	2	164	6.3	6.2	-.8	-3.1		-2.5	0
1610.0	1612.0	B	14.4	5	19.5	3	164	6.3	6.2	-1.4	-4.0		-2.8	0
1612.0	1614.0	C	14.9	286	19.4	3	164	6.3	6.3	-1.1	-3.1		-.3	0
1616.0	1617.1	C	28.8	56	19.3	1	171	6.3	6.3	-.1	-4.1		-4.0	0
1628.5	1630.5	B	36.2	60	19.4	359	171	6.2	6.2	.0	-4.3		-5.5	0
1651.8	1653.3	B	15.4	359	19.2	45	173	6.2	6.2	-1.4	-4.2		-2.1	0
1653.3	1654.5	B	13.8	333	19.1	6	174	6.2	6.2	-1.7	-3.8		-1.5	0
1655.5	1656.5	B	11.2	59	19.1	6	181	6.2	6.2	-1.6	-2.9		-2.9	0
1659.5	1660.5	C	12.4	285	19.1	360	182	6.2	6.2	-2.0	-2.5		-2.5	0
1685.5	1686.5	B	20.4	334	18.9	4	176	6.2	6.2	-3.8	-5.8		-3.1	0
1692.5	1696.5	B	43.3	7	18.9	4	190	6.2	6.2	-0.4	-11.7		-11.7	0
1696.5	1699.5	B	47.9	339	18.9	360	189	6.2	6.2	-10.7	-12.3		-4.5	0
1700.0	1704.0	C	40.8	353	18.8	355	186	6.2	6.2	-7.4	-10.3		-5.0	0
1704.0	1706.5	B	37.5	356	18.9	358	188	6.2	6.2	-6.3	-9.1		-4.3	0
1718.0	1720.0	B	37.7	19	19.2	357	188	6.2	6.2	-1.1	-9.1		-2.0	0
1737.0	1739.0	B	19.7	179	19.0	2	168	6.2	6.3	.0	.1		-.1	0
1755.0	1756.0	C	28.5	3	18.8	2	168	6.3	6.3	-2.8	-6.6		-4.5	0
1757.0	1758.0	C	36.4	359	18.8	3	167	6.3	6.2	-1.2	-8.8		-3.2	0
1761.0	1762.0	B	23.3	358	18.8	4	166	6.3	6.2	-1.4	-5.5		-2.8	0
1765.0	1766.0	C	21.6	25	18.8	4	166	6.3	6.2	-1.7	-4.5		-4.3	0
1766.0	1768.0	C	33.1	1	18.8	4	166	6.3	6.2	-2.1	-7.7		-4.3	0
1768.0	1770.0	B	39.9	8	18.9	6	167	6.3	6.2	-1.8	-9.7		-5.3	0
1774.0	1776.0	B	38.1	327	19.0	0	170	6.2	6.2	-2.6	-8.6		-.5	0
1786.0	1788.0	C	52.7	185	19.2	360	169	6.2	6.3	1.1	3.9		2.4	0
1795.0	1796.0	C	25.6	231	19.3	1	162	6.2	6.3	-1.1	-.9		.9	0
1806.0	1808.0	C	30.7	355	19.3	1	162	6.2	6.3	-2.3	-7.1		-4.2	0
1812.0	1814.0	C	32.3	350	19.3	359	162	6.2	6.3	-3.9	-7.6		-5.4	0
1820.0	1822.0	B	22.8	358	19.3	3	162	6.2	6.3	-1.7	-5.3		-3.5	0
1822.0	1824.0	B	24.8	358	19.3	6	171	6.2	6.3	-3.0	-5.9		-4.0	0
1824.0	1826.0	B	20.9	354	19.3	6	177	6.2	6.2	-2.5	-5.2		-2.7	0
1828.0	1830.0	A	23.9	319	19.3	3	190	6.2	6.2	-3.5	-4.4		-.7	0
1832.0	1834.0	B	28.9	269	19.3	360	174	6.2	6.2	-2.5	-2.5		.9	0
1834.0	1836.0	A	37.6	203	19.3	359	173	6.2	6.2	-.3	1.6		1.5	0
1838.0	1840.0	C	27.6	176	19.4	356	172	6.2	6.2	1.1	.9		1.2	0
1840.0	1842.0	D	28.8	224	19.4	0	168	6.2	6.2	-.5	-.2		1.7	0
1861.0	1862.0	C	14.2	299	19.5	2	165	6.3	6.2	-2.3	-3.4		-1.7	0

CORRELATION INTERVAL	CORR. GRADE	DIP ANG.	DIP AZ.	DRFT ANG.	DRFT AZ.	AZ. NO.1	DIA 13	DIA 24	DISPLACEMENTS					M
									H12	H23	H13	H24	H14	
1863.0	1864.0	B	14.3	226	19.6	1	165	6.3	6.2	-2.1	-1.3	-1.3	-1.3	0
1866.0	1867.0	B	12.3	277	19.6	4	169	6.3	6.2	-1.5	-2.6	-1.7	-1.7	0
1868.0	1870.0	A	3.4	278	19.5	359	179	6.3	6.2	-.7	-2.3	-.3	-.3	0
1873.0	1874.0	B	9.0	260	19.5	358	177	6.3	6.2	-1.7	-2.1	-.7	-.7	0
1875.0	1876.0	A	6.6	226	19.5	359	178	6.3	6.2	-1.0	-1.7	-.5	-.5	0
1877.0	1878.0	A	14.1	307	19.5	360	178	6.3	6.3	-2.1	-3.4	-.8	-.8	0
1879.0	1880.0	A	8.1	241	19.5	357	176	6.3	6.2	-1.3	-1.8	-.5	-.5	0
1882.0	1883.0	A	10.3	219	19.5	3	176	6.3	6.2	-.5	-1.5	-.0	-.0	0
1884.0	1884.3	D	30.2	216	19.5	359	176	6.3	6.2	-2.5	-.5	-.5	-.5	0
1886.0	1887.0	C	27.5	313	19.5	357	176	6.2	6.2	-3.3	-5.3	-.6	-.6	0
1891.0	1892.0	B	20.5	214	19.4	355	177	6.2	6.2	-1.9	-.3	-.5	-.5	0
1893.0	1894.0	B	9.5	322	19.4	358	177	6.2	6.2	-1.5	-3.2	-.9	-.9	0
1895.0	1896.0	A	11.9	307	19.4	358	176	6.2	6.2	-1.8	-3.2	-.8	-.8	0
1898.0	1899.0	B	6.2	211	19.5	358	174	6.2	6.2	-1.2	-1.6	-.9	-.9	0
1900.0	1901.0	C	8.9	229	19.5	357	173	6.2	6.2	-1.5	-1.6	-.8	-.8	0
1906.0	1908.0	D	11.0	296	19.8	359	171	6.2	6.3	-.9	-3.0	-.1	-.1	0
1911.0	1912.0	C	6.7	29	19.9	358	171	6.2	6.3	-.1	-2.9	-.9	-.9	0
1915.0	1916.0	D	7.9	285	20.0	356	165	6.2	6.2	-1.7	-2.7	-1.3	-1.3	0
1917.0	1918.0	C	16.6	152	20.1	1	163	6.2	6.2	-.5	-.3	-.5	-.5	0
1921.0	1922.0	C	12.4	320	20.2	359	162	6.2	6.2	-2.4	-3.7	-2.5	-2.5	0
1924.0	1925.0	A	12.7	305	20.3	6	164	6.2	6.2	-1.5	-3.4	-1.4	-1.4	0
1928.0	1929.0	C	7.5	23	20.5	8	172	6.2	6.2	-1.9	-3.1	-3.0	-3.0	0
1930.0	1932.0	B	19.6	23	20.6	7	172	6.3	6.2	-1.2	-4.8	-3.2	-3.2	0
1932.0	1934.0	B	23.1	32	20.6	6	171	6.3	6.2	-1.8	-5.0	-4.6	-4.6	0
1935.0	1936.0	C	17.1	331	20.6	2	171	6.3	6.2	-2.5	-4.6	-2.2	-2.2	0
1938.0	1940.0	B	21.6	4	20.7	2	172	6.3	6.2	-2.6	-5.6	-3.7	-3.7	0
1942.0	1944.0	B	18.8	2	20.7	2	172	6.3	6.2	-1.7	-5.4	-1.6	-1.6	0
1944.0	1945.0	B	23.4	9	20.7	2	172	6.3	6.2	-1.9	-5.9	-.3	-.3	0
1946.0	1948.0	A	25.4	10	20.7	1	173	6.3	6.2	-1.9	-6.3	-3.4	-3.4	0
1950.0	1952.0	A	20.6	10	20.7	5	173	6.3	6.2	-1.9	-5.6	-3.5	-3.5	0
1954.0	1956.0	D	17.8	358	20.7	9	173	6.3	6.2	-1.9	-4.9	-2.8	-2.8	0
1957.0	1958.0	B	16.7	3	20.7	9	174	6.3	6.2	-1.3	-4.7	-2.3	-2.3	0
1959.0	1960.0	C	12.7	264	20.7	8	174	6.3	6.2	-1.5	-2.3	-.6	-.6	0
1974.0	1975.0	D	6.4	357	20.8	8	189	6.3	6.3	-1.9	-3.2	-1.7	-1.7	0
1976.0	1978.0	B	16.0	310	20.8	6	192	6.3	6.3	-3.4	-3.4	-1.3	-1.3	0
1978.0	1980.0	B	14.5	313	20.9	359	191	6.3	6.2	-2.8	-3.4	-.7	-.7	0
1982.0	1983.0	A	21.6	320	20.9	6	188	6.2	6.2	-3.0	-4.5	-.7	-.7	0
1985.0	1986.0	A	26.5	329	21.0	3	190	6.2	6.2	-4.2	-5.6	-1.3	-1.3	0
1986.0	1988.0	C	23.4	341	21.0	2	190	6.2	6.2	-3.3	-5.6	-1.3	-1.3	0
1989.0	1990.0	B	22.2	329	21.0	2	191	6.2	6.3	-3.6	-4.9	-1.1	-1.1	0
1992.0	1992.2	D	14.5	327	21.0	10	196	6.2	6.3	-4.2	-3.7	-2.5	-2.5	0
2004.0	2006.0	A	42.2	314	21.2	359	231	6.2	6.4	-8.5	-.8	2.0	2.0	0
2010.0	2012.0	H	18.2	336	21.2	1	228	6.2	6.4	-3.9	-2.5	-.5	-.5	0
2014.0	2015.0	A	21.8	329	21.2	358	224	6.2	6.4	-3.8	-2.6	1.2	1.2	0
2018.0	2019.0	A	23.4	311	21.2	1	219	6.2	6.4	-3.9	-2.2	1.0	1.0	0
2026.0	2026.3	B	26.9	35	21.2	7	225	6.2	6.4	-5.9	-6.1	-3.5	-3.5	0
2038.0	2038.4	C	40.2	203	21.2	5	245	6.2	6.4	3.1	2.1	2.0	2.0	0
2041.0	2042.0	C	27.5	225	21.2	7	252	6.2	6.4	2.7	1.7	3.4	3.4	0
2054.0	2055.0	D	20.0	342	21.2	6	263	6.1	6.4	-1.6	-.0	3.8	3.8	0
2069.0	2070.0	C	33.3	305	21.2	8	269	6.1	6.4	-.9	3.5	6.5	6.5	0
2104.0	2105.0	D	21.4	190	21.9	7	259	6.1	6.3	-.1	-.1	-.2	-.2	0
2110.0	2112.0	C	21.8	44	22.0	6	268	6.2	6.4	-4.5	-2.5	-.5	-.5	0
2118.0	2119.0	C	22.4	283	22.1	3	268	6.2	6.4	-.8	2.5	2.6	2.6	0
2120.0	2122.0	C	29.2	211	22.1	2	267	6.2	6.4	3.1	1.5	2.8	2.8	0
2124.0	2126.0	C	5.3	286	22.2	2	265	6.2	6.3	-1.5	-.3	1.3	1.3	0

CORRELATION INTERVAL	CORR. GRADE	DIP ANG.	DIP AZ.	DRFT ANG.	DRFT AZ.	AZ. NO.1	DIA 13	DIA 24	DISPLACEMENTS					M
									H12	H23	H13	H24	H14	
2128.0	2130.0	A	15.8	344	22.2	3	265	6.2	6.4	-3.3	.0		1.6	0
2132.0	2133.0	C	52.4	205	22.3	6	264	6.2	6.4	2.7	2.5		-.3	0
2142.0	2144.0	B	13.8	227	22.4	7	265	6.1	6.4	-.2	.7		1.3	0
2148.0	2150.0	A	8.6	305	22.5	7	264	6.1	6.3	-1.6	.2		1.7	0
2154.0	2156.0	C	13.3	40	22.6	6	264	6.1	6.3	-2.6	-1.6		1.3	0
2158.0	2160.0	A	13.7	313	22.6	7	265	6.1	6.3	-1.9	.6		2.1	0
2162.0	2164.0	A	12.9	300	22.7	8	274	6.1	6.3	-1.7	1.2		1.7	0
2165.0	2166.0	A	11.8	266	22.7	5	274	6.1	6.3	-.9	1.3		1.5	0
2167.0	2168.0	B	21.6	297	22.7	5	273	6.1	6.3	-1.2	2.5		2.7	0
2169.0	2170.0	A	15.9	296	22.7	4	270	6.1	6.3	-1.1	1.6		2.5	0
2171.0	2172.0	A	19.1	308	22.7	5	270	6.1	6.2	-1.2	1.7		3.1	0
2174.0	2175.0	A	6.6	309	22.7	5	276	6.1	6.3	-1.3	.7		1.8	0
2176.0	2177.0	A	3.8	323	22.8	5	275	6.1	6.3	-1.3	.3		1.7	0
2181.0	2182.0	A	8.4	308	22.8	6	273	6.1	6.3	-1.4	.7		1.9	0
2185.0	2186.0	A	9.8	333	22.8	6	274	6.1	6.3	-1.6	.5		2.2	0
2188.0	2190.0	A	2.4	286	22.9	3	274	6.1	6.2	-1.0	.3		1.7	0
2190.0	2192.0	A	7.3	342	22.9	2	268	6.1	6.3	-1.9	.1		1.7	0
2193.0	2194.0	A	14.7	339	22.9	5	265	6.1	6.3	-2.3	.1		2.4	0
2195.0	2196.0	A	12.6	345	22.9	6	266	6.1	6.3	-2.2	-.2		2.2	0
2197.0	2198.0	A	8.4	231	22.9	7	266	6.1	6.3	-1.0	.3		1.0	0
2199.0	2200.0	B	16.7	332	22.9	5	267	6.1	6.3	-1.6	.5		3.3	0
2201.0	2202.0	C	22.0	163	22.9	3	265	6.1	6.3	-1.5	.0		1.6	0
2202.0	2203.0	B	8.6	319	23.0	5	261	6.1	6.3	-2.4	-.1		1.2	0
2204.0	2205.0	B	17.3	336	23.0	6	260	6.1	6.5	-2.5	-.2		2.7	0
2207.0	2208.0	A	17.1	290	23.0	8	262	6.1	6.4	-1.5	1.1		2.2	0
2211.0	2212.0	A	10.8	327	23.0	7	264	6.1	6.4	-1.5	.0		2.5	0
2215.0	2216.0	B	19.1	217	23.1	8	265	6.1	6.4	-1.2	.8		3.1	0
2217.0	2219.0	B	11.0	298	23.1	4	265	6.1	6.4	-1.5	.7		2.0	0
2221.0	2222.0	A	11.3	334	23.1	5	264	6.1	6.3	-1.9	.0		2.2	0
2223.0	2224.0	A	16.6	320	23.1	9	264	6.1	6.3	-2.0	.5		2.6	0
2227.0	2228.0	A	17.2	319	23.1	11	274	6.1	6.4	-1.7	1.2		2.8	0
2229.0	2230.0	B	18.0	284	23.1	11	278	6.1	6.4	.3	2.0		3.3	0
2231.0	2232.0	A	16.5	320	23.1	9	277	6.1	6.4	-1.1	1.5		3.3	0
2235.0	2236.0	A	12.1	331	23.1	10	276	6.1	6.3	-1.7	.7		2.4	0
2237.0	2238.0	B	15.8	315	23.1	8	276	6.1	6.3	-1.2	1.5		2.9	0
2241.0	2242.0	C	14.7	316	23.1	9	279	6.1	6.4	-1.5	1.5		2.5	0
2243.0	2244.0	B	11.8	339	23.1	7	280	6.1	6.4	-1.7	.9		2.5	0
2246.0	2247.0	A	20.0	341	23.1	10	280	6.1	6.4	-2.3	1.4		3.2	0
2251.0	2252.0	C	16.0	294	23.2	6	282	6.1	6.4	-1.5	2.2		1.7	0
2255.0	2256.0	H	11.2	317	23.2	3	282	6.1	6.4	-.7	1.6		2.9	0
2259.0	2260.0	C	10.8	291	23.2	6	281	6.1	6.4	1.3	1.5		4.3	0
2261.0	2262.0	C	17.3	355	23.2	5	281	6.1	6.4	-2.0	1.0		3.3	0
2267.0	2268.0	C	15.7	5	23.2	2	279	6.1	6.4	-2.0	.5		3.1	0
2269.0	2270.0	B	16.9	354	23.2	5	276	6.1	6.4	-2.1	.5		3.2	0
2273.0	2274.0	C	16.2	353	23.2	3	267	6.1	6.4	-1.9	-.2		3.3	0
2275.0	2276.0	B	21.0	332	23.2	2	264	6.1	6.2	-2.1	.7		3.6	0
2280.0	2281.0	B	8.1	16	23.1	5	254	6.1	6.2	-2.3	-1.5		1.1	0
2283.0	2284.0	B	10.4	7	23.1	6	254	6.1	6.2	-2.9	-1.5		.9	0
2287.0	2288.0	A	5.3	5	23.1	6	254	6.1	6.4	-2.5	-1.2		.7	0
2289.0	2290.0	B	6.9	199	23.0	6	254	6.1	6.4	-1.0	-.5		.8	0
2290.0	2291.0	B	1.5	83	23.0	5	254	6.1	6.4	-1.8	-1.1		.7	0
2292.0	2293.0	C	7.0	45	23.0	4	254	6.2	6.3	-2.4	-1.7		.6	0
2295.0	2296.0	B	9.2	277	23.0	14	256	6.2	6.2	-1.5	-.2		1.2	0
2297.0	2298.0	C	14.7	7	23.0	9	257	6.2	6.4	-2.7	-1.7		1.9	0
2299.0	2300.0	C	14.6	328	23.1	10	257	6.2	6.4	-2.4	-.4		2.1	0

THE FOLLOWING PARAMETERS APPLY TO THE LOG FROM 466.0 FEET TO 2408.0

MAGNETIC DECLINATION IS 20.0 DEGREES.

4.0 FEET WERE ADDED TO THE DIP LOG TO CORRECT DEPTH TO THE BASE LOG DEPTH.

DRIFT AZIMUTH AND AZIMUTH OF NO. 1 ARM HAVE BEEN CORRECTED TO TRUE NORTH IN THIS PRESENTATION.



A. J. ...

When done, we guarantee the accuracy of any interpretation of log data, correction of log data to present scale standards, or computations, or illustrations prepared by Vision personnel or which may appear on this log, or in any other work, the nature of such work, interpretations, conversions, or computations makes such Vision is not responsible, except where due to gross negligence or wilful misconduct, for any loss, damage, or expense sustained from the use thereof.