# DIP LOG CALCULATIONS

| | | | |
|---|---|---|---|
| **COMPANY** | REICHHOLD ENERGY CORPORATION | | |
| **WELL** | DSC-LONGVIEW FIBRE NO. 1 | | |
| **FIELD** | NEHALEM BASIN | | |
| **COUNTY** | COLUMBIA | **STATE** | OREGON |

WELEX

A Halliburton Company

16061

| CORRELATION INTERVAL | | CORR. GRADE | DIP ANGLE | DIP AZ. | DRFT ANGLE | DRFT AZ. | AZ. NO.1 | DIA 13 | DISPLACEMENTS NO.1 | NO.2 | NO.3 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 400.0 | 401.0 | C | 12.2 | 7. | 0.1 | 59. | 353. | 9.9 | 0.0 | 1.70 | 1.50 |
| 402.0 | 403.0 | C | 9.5 | 341. | 0.1 | 61. | 351. | 9.7 | 0.0 | 1.40 | 0.70 |
| 410.0 | 412.0 | C | 10.7 | 332. | 0.1 | 134. | 44. | 8.0 | 0.0 | 0.60 | -0.70 |
| 412.0 | 414.0 | B | 1.3 | 4. | 0.1 | 136. | 45. | 6.4 | 0.0 | 0.10 | 0.0 |
| 416.0 | 417.0 | B | 6.6 | 354. | 0.1 | 139. | 52. | 6.2 | 0.0 | 0.40 | -0.20 |
| 418.0 | 420.0 | C | 11.5 | 320. | 0.1 | 147. | 64. | 6.3 | 0.0 | -0.10 | -1.00 |
| 422.0 | 423.0 | C | 10.3 | 325. | 0.1 | 154. | 70. | 6.3 | 0.0 | -0.10 | -0.90 |
| 426.0 | 428.0 | B | 9.5 | 332. | 0.1 | 180. | 90. | 6.4 | 0.0 | -0.30 | -0.90 |
| 428.0 | 430.0 | C | 13.9 | 346. | 0.1 | 188. | 97. | 6.4 | 0.0 | -0.30 | -1.30 |
| 430.0 | 432.0 | D | 6.4 | 340. | 0.1 | 188. | 97. | 6.4 | 0.0 | -0.20 | -0.60 |
| 432.0 | 434.0 | D | 9.5 | 343. | 0.1 | 193. | 101. | 6.4 | 0.0 | -0.30 | -0.90 |
| 434.0 | 436.0 | B | 5.5 | 319. | 0.1 | 199. | 106. | 6.4 | 0.0 | -0.40 | -0.50 |
| 436.0 | 437.0 | C | 3.1 | 295. | 0.1 | 204. | 111. | 6.4 | 0.0 | -0.30 | -0.20 |
| 437.0 | 438.7 | B | 3.2 | 336. | 0.1 | 208. | 114. | 6.3 | 0.0 | -0.20 | -0.30 |
| 449.0 | 450.0 | B | 12.2 | 353. | 0.1 | 209. | 142. | 6.3 | 0.0 | -0.90 | -1.10 |
| 450.0 | 452.0 | C | 13.4 | 13. | 0.1 | 211. | 149. | 6.4 | 0.0 | -0.80 | -1.30 |
| 452.0 | 454.0 | C | 6.6 | 314. | 0.1 | 219. | 163. | 6.4 | 0.0 | -0.60 | -0.10 |
| 458.0 | 460.0 | D | 5.5 | 298. | 0.1 | 246. | 206. | 6.3 | 0.0 | -0.10 | 0.40 |
| 460.0 | 462.0 | B | 7.4 | 332. | 0.1 | 263. | 225. | 6.2 | 0.0 | -0.30 | 0.40 |
| 462.0 | 463.0 | B | 3.2 | 276. | 0.1 | 274. | 236. | 6.2 | 0.0 | 0.20 | 0.30 |
| 465.0 | 466.0 | D | 13.5 | 64. | 0.1 | 288. | 250. | 6.3 | 0.0 | -1.30 | -0.70 |
| 484.0 | 485.0 | D | 23.2 | 12. | 0.2 | 334. | 314. | 6.2 | 0.0 | 0.90 | 2.30 |
| 485.0 | 486.0 | A | 18.2 | 322. | 0.2 | 333. | 311. | 6.3 | 0.0 | 1.70 | 1.40 |
| 486.0 | 488.0 | C | 11.7 | 331. | 0.1 | 337. | 310. | 6.4 | 0.0 | 1.00 | 1.00 |
| 492.0 | 494.3 | B | 15.9 | 12. | 0.1 | 31. | 348. | 6.3 | 0.0 | 1.30 | 1.40 |
| 494.3 | 495.0 | A | 15.4 | 24. | 0.1 | 41. | 356. | 6.3 | 0.0 | 1.20 | 1.40 |
| 496.0 | 498.0 | D | 19.3 | 355. | 0.1 | 40. | 352. | 6.4 | 0.0 | 1.90 | 1.30 |
| 504.0 | 506.0 | C | 13.8 | 319. | 0.1 | 31. | 346. | 6.4 | 0.0 | 1.30 | 0.30 |
| 511.0 | 513.0 | D | 32.0 | 299. | 0.1 | 30. | 348. | 6.3 | 0.0 | 2.60 | -0.60 |
| 521.0 | 522.0 | D | 8.8 | 122. | 0.0 | 22. | 348. | 6.5 | 0.0 | -0.70 | 0.10 |
| 536.0 | 538.0 | D | 2.4 | 255. | 0.0 | 27. | 354. | 6.4 | 0.0 | 0.0 | -0.20 |
| 542.0 | 544.0 | D | 9.9 | 175. | 0.1 | 50. | 21. | 6.3 | 0.0 | -0.90 | -0.20 |
| 544.0 | 546.0 | D | 14.0 | 1. | 0.0 | 55. | 27. | 6.3 | 0.0 | 1.30 | 0.30 |
| 548.5 | 550.0 | A | 1.1 | 56. | 0.1 | 66. | 38. | 6.3 | 0.0 | 0.10 | 0.10 |
| 558.0 | 560.0 | C | 26.6 | 247. | 0.3 | 100. | 72. | 6.3 | 0.0 | -2.70 | -1.50 |
| 564.0 | 565.0 | C | 15.2 | 277. | 0.2 | 121. | 79. | 6.2 | 0.0 | -1.30 | -1.20 |
| 565.0 | 567.0 | D | 15.3 | 295. | 0.1 | 120. | 75. | 6.5 | 0.0 | -1.00 | -1.50 |
| 568.0 | 570.0 | D | 20.5 | 289. | 0.2 | 121. | 74. | 6.5 | 0.0 | -1.50 | -2.00 |
| 571.5 | 572.5 | D | 15.6 | 270. | 0.1 | 122. | 72. | 6.5 | 0.0 | -1.40 | -1.30 |
| 573.0 | 575.0 | D | 10.5 | 269. | 0.1 | 124. | 68. | 6.5 | 0.0 | -0.90 | -0.90 |
| 578.0 | 580.0 | D | 15.5 | 261. | 0.2 | 127. | 74. | 6.5 | 0.0 | -1.50 | -1.10 |
| 580.0 | 582.0 | D | 11.2 | 239. | 0.3 | 132. | 75. | 6.5 | 0.0 | -1.10 | -0.40 |
| 588.0 | 590.0 | D | 14.5 | 270. | 0.2 | 136. | 72. | 6.5 | 0.0 | -1.30 | -1.20 |
| 590.0 | 592.0 | D | 19.7 | 282. | 0.2 | 141. | 69. | 6.5 | 0.0 | -1.50 | -1.90 |
| 594.0 | 596.0 | D | 23.6 | 257. | 0.2 | 154. | 67. | 6.4 | 0.0 | -2.30 | -1.80 |
| 597.0 | 598.0 | D | 17.9 | 276. | 0.2 | 164. | 71. | 6.4 | 0.0 | -1.50 | -1.60 |
| 600.0 | 601.0 | C | 10.5 | 312. | 0.2 | 176. | 80. | 6.3 | 0.0 | -0.50 | -1.00 |
| 602.0 | 604.0 | D | 18.5 | 281. | 0.3 | 184. | 85. | 6.4 | 0.0 | -1.70 | -1.50 |
| 604.0 | 606.0 | B | 19.1 | 287. | 0.3 | 192. | 94. | 6.4 | 0.0 | -1.80 | -1.50 |
| 608.0 | 610.0 | D | 19.0 | 297. | 0.2 | 212. | 117. | 6.4 | 0.0 | -1.90 | -1.20 |
| 610.0 | 612.0 | D | 16.9 | 290. | 0.2 | 220. | 128. | 6.5 | 0.0 | -1.70 | -0.60 |
| 612.0 | 614.0 | D | 20.6 | 298. | 0.1 | 228. | 135. | 6.5 | 0.0 | -2.10 | -0.80 |
| 614.0 | 616.0 | D | 12.1 | 284. | 0.1 | 232. | 138. | 6.5 | 0.0 | -1.10 | -0.10 |
| 616.0 | 618.0 | D | 14.3 | 300. | 0.1 | 235. | 143. | 6.5 | 0.0 | -1.40 | -0.40 |
| 618.0 | 620.0 | D | 12.8 | 301. | 0.1 | 241. | 151. | 6.5 | 0.0 | -1.20 | -0.20 |

| CORRELATION INTERVAL | | CORR. GRADE | DIP ANGLE | DIP AZ. | DRFT ANGLE | DRFT AZ. | DIA NO.1 | DIA 13 | DISPLACEMENTS NO.1 | NO.2 | NO.3 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 626.0 | 628.0 | D | 17.0 | 268. | 0.1 | 252. | 177. | 6.4 | 0.0 | -0.30 | 1.30 |
| 630.0 | 632.0 | D | 9.6 | 294. | 0.0 | 281. | 213. | 6.3 | 0.0 | 0.0 | 0.80 |
| 634.0 | 636.0 | D | 27.5 | 289. | 0.1 | 304. | 239. | 6.4 | 0.0 | 1.50 | 2.90 |
| 636.0 | 638.0 | C | 16.4 | 287. | 0.1 | 312. | 248. | 6.4 | 0.0 | 1.10 | 1.60 |
| 640.0 | 644.0 | D | 22.6 | 275. | 0.0 | 297. | 228. | 6.4 | 0.0 | 1.30 | 2.30 |
| 644.0 | 646.0 | D | 22.2 | 279. | 0.0 | 311. | 248. | 6.3 | 0.0 | 1.70 | 2.10 |
| 646.0 | 648.0 | A | 25.6 | 290. | 0.0 | 319. | 256. | 6.3 | 0.0 | 1.90 | 2.50 |
| 656.0 | 657.0 | A | 21.6 | 293. | 0.0 | 308. | 256. | 6.3 | 0.0 | 1.50 | 2.10 |
| 659.0 | 660.0 | B | 26.2 | 303. | 0.0 | 304. | 271. | 6.2 | 0.0 | 2.00 | 2.50 |
| 664.0 | 664.5 | B | 26.4 | 280. | 0.0 | 326. | 285. | 6.3 | 0.0 | 2.70 | 1.50 |
| 665.0 | 667.0 | C | 28.9 | 262. | 0.0 | 329. | 287. | 6.1 | 0.0 | 2.80 | 0.70 |
| 672.0 | 673.0 | C | 16.3 | 305. | 0.1 | 338. | 310. | 6.3 | 0.0 | 1.60 | 0.90 |
| 680.0 | 682.0 | C | 13.4 | 287. | 0.1 | 305. | 284. | 6.4 | 0.0 | 1.30 | 0.90 |
| 686.0 | 688.0 | D | 21.7 | 275. | 0.0 | 333. | 281. | 6.4 | 0.0 | 2.20 | 1.20 |
| 688.0 | 690.0 | D | 13.7 | 241. | 0.0 | 338. | 284. | 6.3 | 0.0 | 1.10 | -0.10 |
| 704.0 | 706.0 | D | 13.8 | 228. | 0.0 | 296. | 254. | 6.4 | 0.0 | 1.30 | 0.30 |
| 706.0 | 708.0 | C | 16.3 | 246. | 0.0 | 304. | 263. | 6.4 | 0.0 | 1.60 | 0.60 |
| 708.0 | 710.0 | B | 14.2 | 262. | 0.0 | 314. | 271. | 6.4 | 0.0 | 1.40 | 0.70 |
| 711.0 | 712.0 | D | 7.6 | 220. | 0.1 | 319. | 276. | 6.3 | 0.0 | 0.50 | -0.20 |
| 713.0 | 714.2 | A | 14.0 | 236. | 0.2 | 325. | 280. | 6.2 | 0.0 | 1.10 | -0.10 |
| 716.0 | 718.0 | B | 6.4 | 217. | 0.2 | 334. | 287. | 6.3 | 0.0 | 0.30 | -0.30 |
| 719.0 | 720.0 | B | 10.4 | 250. | 0.1 | 339. | 320. | 6.3 | 0.0 | 0.50 | -0.50 |
| 721.0 | 722.0 | B | 4.3 | 257. | 0.0 | 34. | 342. | 6.4 | 0.0 | 0.10 | -0.30 |
| 724.0 | 725.0 | A | 9.5 | 242. | 0.0 | 46. | 0. | 6.3 | 0.0 | -0.30 | -0.90 |
| 730.0 | 732.0 | C | 7.9 | 269. | 0.0 | 56. | 0. | 6.3 | 0.0 | 0.10 | -0.60 |
| 734.0 | 736.0 | D | 2.1 | 291. | 0.1 | 62. | 1. | 6.5 | 0.0 | 0.10 | -0.10 |
| 736.0 | 738.0 | C | 3.5 | 103. | 0.0 | 56. | 202. | 6.5 | 0.0 | 0.0 | -0.30 |
| 738.0 | 740.0 | C | 6.6 | 244. | 0.0 | 55. | 352. | 6.4 | 0.0 | -0.10 | -0.60 |
| 740.0 | 742.0 | C | 5.2 | 214. | 0.0 | 57. | 350. | 6.4 | 0.0 | -0.30 | -0.50 |
| 746.0 | 748.0 | B | 9.0 | 182. | 0.2 | 63. | 354. | 6.1 | 0.0 | -0.80 | -0.60 |
| 754.5 | 755.5 | C | 9.7 | 223. | 0.1 | 86. | 9. | 6.4 | 0.0 | -0.70 | -0.90 |
| 756.8 | 757.2 | C | 9.4 | 190. | 0.1 | 91. | 15. | 6.3 | 0.0 | -0.90 | -0.50 |
| 758.0 | 758.5 | D | 7.9 | 227. | 0.1 | 93. | 18. | 6.3 | 0.0 | -0.60 | -0.70 |
| 762.0 | 764.0 | D | 8.5 | 285. | 0.0 | 117. | 38. | 6.4 | 0.0 | -0.20 | -0.80 |
| 766.0 | 768.0 | C | 8.5 | 294. | 0.0 | 140. | 79. | 6.4 | 0.0 | -0.60 | -0.80 |
| 768.0 | 770.0 | D | 7.9 | 289. | 0.0 | 158. | 104. | 6.0 | 0.0 | -0.70 | -0.50 |
| 771.0 | 773.0 | B | 2.2 | 354. | 0.0 | 180. | 123. | 6.1 | 0.0 | -0.10 | -0.20 |
| 778.0 | 779.2 | A | 6.2 | 210. | 0.0 | 216. | 159. | 6.4 | 0.0 | 0.30 | 0.60 |
| 786.0 | 788.0 | D | 10.6 | 268. | 0.0 | 200. | 157. | 6.2 | 0.0 | -0.50 | 0.50 |
| 788.0 | 790.0 | D | 8.6 | 283. | 0.0 | 192. | 164. | 6.2 | 0.0 | -0.50 | 0.30 |
| 796.0 | 797.0 | A | 17.6 | 262. | 0.0 | 233. | 203. | 5.9 | 0.0 | 0.60 | 1.60 |
| 800.0 | 801.0 | A | 22.3 | 264. | 0.0 | 236. | 209. | 6.5 | 0.0 | 1.00 | 2.30 |
| 802.0 | 804.0 | D | 18.9 | 256. | 0.0 | 236. | 214. | 6.5 | 0.0 | 1.20 | 1.90 |
| 806.0 | 808.0 | C | 14.4 | 244. | 0.0 | 223. | 202. | 6.4 | 0.0 | 0.90 | 1.40 |
| 810.0 | 812.0 | A | 9.2 | 250. | 0.0 | 221. | 203. | 6.4 | 0.0 | 0.50 | 0.90 |
| 815.0 | 817.0 | C | 11.3 | 257. | 0.1 | 225. | 221. | 6.5 | 0.0 | 0.80 | 1.10 |
| 818.0 | 819.0 | B | 10.0 | 248. | 0.1 | 219. | 221. | 6.4 | 0.0 | 0.80 | 0.90 |
| 819.0 | 820.0 | B | 11.2 | 236. | 0.0 | 219. | 220. | 6.4 | 0.0 | 1.00 | 0.90 |
| 821.0 | 822.0 | D | 10.5 | 249. | 0.0 | 209. | 211. | 6.4 | 0.0 | 0.70 | 1.00 |
| 824.0 | 826.0 | D | 8.9 | 244. | 0.0 | 203. | 216. | 6.4 | 0.0 | 0.70 | 0.80 |
| 826.0 | 827.0 | B | 5.2 | 220. | 0.0 | 207. | 222. | 6.4 | 0.0 | 0.50 | 0.30 |
| 827.0 | 828.0 | B | 3.2 | 209. | 0.0 | 211. | 229. | 6.4 | 0.0 | 0.30 | 0.10 |
| 828.0 | 830.0 | D | 5.5 | 262. | 0.0 | 212. | 230. | 6.4 | 0.0 | 0.40 | 0.50 |
| 836.0 | 838.0 | A | 11.1 | 251. | 0.0 | 216. | 225. | 6.5 | 0.0 | 0.90 | 1.00 |
| 839.0 | 840.0 | A | 11.1 | 259. | 0.0 | 213. | 233. | 6.5 | 0.0 | 0.90 | 1.00 |

| CORRELATION INTERVAL | | CORR. GRADE | DIP ANGLE | DIP AZ. | DRFT ANGLE | DRFT AZ. | AZ. NO.1 | DIA 13 | DISPLACEMENTS NO.1 | NO.2 | NO.3 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 840.0 | 842.0 | C | 9.9 | 262. | 0.0 | 213. | 235. | 6.5 | 0.0 | 0.80 | 0.90 |
| 842.0 | 844.0 | C | 10.6 | 254. | 0.0 | 211. | 233. | 6.4 | 0.0 | 0.90 | 0.90 |
| 844.0 | 846.0 | B | 8.3 | 250. | 0.0 | 206. | 229. | 6.4 | 0.0 | 0.70 | 0.70 |
| 846.0 | 847.3 | C | 7.8 | 259. | 0.0 | 205. | 230. | 6.4 | 0.0 | 0.60 | 0.70 |
| 849.0 | 850.0 | B | 11.0 | 270. | 0.1 | 211. | 243. | 6.5 | 0.0 | 0.90 | 1.00 |
| 850.0 | 851.0 | D | 9.0 | 243. | 0.1 | 214. | 248. | 6.5 | 0.0 | 0.90 | 0.50 |
| 853.0 | 854.0 | A | 9.7 | 277. | 0.0 | 220. | 244. | 6.4 | 0.0 | 0.70 | 0.90 |
| 854.0 | 855.0 | B | 10.8 | 273. | 0.0 | 218. | 241. | 6.4 | 0.0 | 0.80 | 1.00 |
| 856.0 | 857.3 | A | 8.2 | 296. | 0.0 | 218. | 245. | 6.4 | 0.0 | 0.40 | 0.80 |
| 864.0 | 865.2 | C | 5.3 | 297. | 0.0 | 234. | 253. | 6.3 | 0.0 | 0.30 | 0.50 |
| 865.2 | 867.0 | C | 5.6 | 291. | 0.0 | 237. | 259. | 6.2 | 0.0 | 0.40 | 0.50 |
| 867.0 | 869.0 | A | 5.0 | 214. | 0.0 | 235. | 253. | 6.1 | 0.0 | 0.40 | 0.0 |
| 869.0 | 870.0 | A | 6.0 | 267. | 0.0 | 224. | 246. | 6.3 | 0.0 | 0.50 | 0.50 |
| 870.0 | 872.0 | B | 5.9 | 266. | 0.0 | 218. | 245. | 6.4 | 0.0 | 0.50 | 0.50 |
| 872.0 | 873.0 | A | 6.6 | 280. | 0.0 | 217. | 250. | 6.4 | 0.0 | 0.50 | 0.60 |
| 876.0 | 877.5 | C | 6.4 | 126. | 0.0 | 216. | 255. | 6.2 | 0.0 | -0.30 | -0.60 |
| 877.5 | 878.4 | B | 3.6 | 161. | 0.0 | 218. | 260. | 6.3 | 0.0 | 0.0 | -0.30 |
| 879.5 | 881.5 | C | 11.4 | 297. | 0.0 | 206. | 249. | 6.3 | 0.0 | 0.60 | 1.10 |
| 889.0 | 890.0 | D | 15.9 | 119. | 0.0 | 249. | 293. | 6.3 | 0.0 | -1.50 | -1.10 |
| 890.5 | 891.0 | D | 5.4 | 216. | 0.0 | 251. | 292. | 6.2 | 0.0 | 0.20 | -0.30 |
| 894.0 | 896.0 | D | 5.4 | 101. | 0.0 | 252. | 283. | 6.2 | 0.0 | -0.50 | -0.30 |
| 906.0 | 908.0 | D | 13.7 | 269. | 0.1 | 265. | 295. | 6.4 | 0.0 | 1.30 | 0.30 |
| 908.0 | 909.0 | A | 11.5 | 270. | 0.1 | 270. | 294. | 6.4 | 0.0 | 1.10 | 0.30 |
| 909.5 | 910.3 | B | 7.8 | 258. | 0.0 | 268. | 289. | 6.4 | 0.0 | 0.70 | 0.10 |
| 910.3 | 912.0 | D | 11.9 | 258. | 0.0 | 268. | 287. | 6.4 | 0.0 | 1.10 | 0.20 |
| 912.0 | 914.0 | D | 13.1 | 231. | 0.0 | 264. | 279. | 6.4 | 0.0 | 1.00 | -0.20 |
| 914.0 | 916.0 | C | 13.5 | 235. | 0.0 | 257. | 278. | 6.4 | 0.0 | 1.10 | -0.10 |
| 916.0 | 917.0 | C | 4.3 | 261. | 0.0 | 253. | 286. | 6.4 | 0.0 | 0.40 | 0.10 |
| 917.0 | 918.0 | D | 8.9 | 243. | 0.0 | 254. | 289. | 6.4 | 0.0 | 0.70 | -0.10 |
| 918.0 | 920.0 | D | 12.7 | 239. | 0.0 | 246. | 292. | 6.4 | 0.0 | 0.90 | -0.30 |
| 924.0 | 926.0 | C | 14.8 | 207. | 0.1 | 204. | 302. | 6.3 | 0.0 | 0.10 | -1.20 |
| 926.0 | 928.0 | C | 15.6 | 196. | 0.1 | 185. | 299. | 6.4 | 0.0 | -0.10 | -1.40 |
| 928.0 | 930.0 | C | 16.6 | 210. | 0.2 | 172. | 299. | 6.5 | 0.0 | 0.30 | -1.30 |
| 930.0 | 932.0 | C | 6.3 | 210. | 0.3 | 159. | 299. | 6.5 | 0.0 | 0.10 | -0.50 |
| 932.0 | 934.0 | B | 14.6 | 217. | 0.4 | 146. | 303. | 6.4 | 0.0 | 0.30 | -1.10 |
| 934.0 | 936.0 | C | 9.5 | 228. | 0.4 | 139. | 313. | 6.4 | 0.0 | 0.20 | -0.70 |
| 938.5 | 940.0 | B | 18.9 | 241. | 0.3 | 147. | 342. | 6.4 | 0.0 | -0.10 | -1.70 |
| 940.0 | 942.0 | B | 13.7 | 237. | 0.3 | 150. | 348. | 6.4 | 0.0 | -0.30 | -1.30 |
| 942.0 | 944.0 | B | 17.9 | 229. | 0.3 | 155. | 350. | 6.4 | 0.0 | -0.70 | -1.80 |
| 944.0 | 945.7 | A | 16.9 | 230. | 0.2 | 157. | 0. | 6.4 | 0.0 | -0.90 | -1.70 |
| 945.7 | 948.0 | C | 15.8 | 217. | 0.2 | 161. | 5. | 6.4 | 0.0 | -1.20 | -1.50 |
| 948.0 | 950.0 | A | 14.5 | 241. | 0.1 | 171. | 10. | 6.2 | 0.0 | -0.70 | -1.40 |
| 950.0 | 952.0 | C | 12.3 | 271. | 0.1 | 172. | 10. | 6.1 | 0.0 | 0.0 | -1.00 |
| 952.0 | 953.0 | C | 9.6 | 252. | 0.1 | 167. | 10. | 6.2 | 0.0 | -0.30 | -0.90 |
| 953.0 | 954.0 | C | 11.7 | 260. | 0.1 | 166. | 14. | 6.3 | 0.0 | -0.30 | -1.10 |
| 954.0 | 956.0 | C | 4.2 | 178. | 0.1 | 168. | 23. | 6.4 | 0.0 | -0.40 | -0.10 |
| 956.0 | 957.0 | A | 13.5 | 272. | 0.0 | 171. | 28. | 6.4 | 0.0 | -0.40 | -1.30 |
| 957.0 | 958.2 | B | 11.2 | 260. | 0.0 | 171. | 26. | 6.4 | 0.0 | -0.50 | -1.10 |
| 958.3 | 960.0 | B | 7.8 | 219. | 0.0 | 160. | 26. | 6.4 | 0.0 | -0.70 | -0.60 |
| 960.0 | 961.0 | B | 14.0 | 139. | 0.0 | 154. | 28. | 6.5 | 0.0 | -0.70 | 0.70 |
| 966.0 | 968.0 | D | 19.1 | 267. | 0.1 | 156. | 27. | 6.4 | 0.0 | -0.70 | -1.90 |
| 972.0 | 974.0 | D | 15.1 | 276. | 0.1 | 160. | 22. | 6.5 | 0.0 | -0.20 | -1.40 |
| 974.0 | 976.0 | C | 13.6 | 268. | 0.2 | 165. | 19. | 6.5 | 0.0 | -0.30 | -1.30 |
| 978.0 | 979.0 | A | 15.7 | 270. | 0.2 | 171. | 12. | 6.4 | 0.0 | -0.10 | -1.40 |
| 980.0 | 981.0 | A | 17.8 | 267. | 0.1 | 174. | 15. | 6.5 | 0.0 | -0.30 | -1.70 |

| CORRELATION INTERVAL | | CORR. GRADE | DIP ANGLE | DIP AZ. | DRFT ANGLE | DRFT AZ. | DIA NO.1 | DIA 13 | DISPLACEMENTS NO.1 | NO.2 | NO.3 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 981.0 | 982.0 | B | 17.8 | 268. | 0.1 | 176. | 16. | 6.5 | 0.0 | -0.30 | -1.70 |
| 983.0 | 983.2 | C | 17.8 | 269. | 0.1 | 178. | 17. | 6.5 | 0.0 | -0.30 | -1.70 |
| 984.0 | 986.0 | D | 19.8 | 268. | 0.1 | 175. | 18. | 6.4 | 0.0 | -0.40 | -1.90 |
| 986.0 | 988.0 | D | 16.8 | 279. | 0.2 | 174. | 21. | 6.4 | 0.0 | -0.10 | -1.50 |
| 988.0 | 990.0 | D | 10.1 | 253. | 0.2 | 171. | 21. | 6.4 | 0.0 | -0.50 | -1.00 |
| 990.0 | 991.0 | B | 13.5 | 285. | 0.2 | 165. | 19. | 6.4 | 0.0 | 0.10 | -1.10 |
| 994.0 | 996.0 | B | 17.2 | 260. | 0.2 | 158. | 15. | 6.5 | 0.0 | -0.50 | -1.70 |
| 996.0 | 998.0 | A | 17.5 | 266. | 0.3 | 152. | 11. | 6.4 | 0.0 | -0.20 | -1.60 |
| 998.0 | 999.8 | B | 20.4 | 266. | 0.2 | 148. | 7. | 6.3 | 0.0 | -0.10 | -1.80 |
| 999.8 | 1000.2 | B | 16.6 | 259. | 0.2 | 148. | 4. | 6.3 | 0.0 | -0.20 | -1.50 |
| 1006.0 | 1006.5 | B | 15.6 | 288. | 0.2 | 137. | 23. | 6.5 | 0.0 | 0.10 | -1.30 |
| 1014.0 | 1016.0 | C | 12.6 | 279. | 0.1 | 115. | 32. | 6.5 | 0.0 | -0.30 | -1.20 |
| 1016.0 | 1018.0 | B | 12.3 | 285. | 0.1 | 136. | 59. | 6.4 | 0.0 | -0.70 | -1.20 |
| 1018.0 | 1020.0 | B | 11.4 | 286. | 0.1 | 165. | 79. | 6.3 | 0.0 | -0.90 | -1.00 |
| 1020.0 | 1022.0 | C | 11.5 | 271. | 0.2 | 175. | 84. | 6.4 | 0.0 | -1.10 | -0.80 |
| 1022.0 | 1024.0 | B | 23.3 | 275. | 0.1 | 183. | 88. | 6.4 | 0.0 | -2.30 | -1.70 |
| 1026.0 | 1027.0 | A | 12.0 | 312. | 0.1 | 195. | 111. | 6.3 | 0.0 | -1.00 | -1.00 |
| 1027.0 | 1029.0 | B | 9.6 | 285. | 0.1 | 202. | 124. | 6.2 | 0.0 | -0.90 | -0.30 |
| 1029.0 | 1030.5 | B | 7.5 | 324. | 0.1 | 200. | 122. | 6.1 | 0.0 | -0.60 | -0.60 |
| 1032.0 | 1034.0 | B | 9.0 | 277. | 0.1 | 223. | 142. | 6.3 | 0.0 | -0.70 | 0.10 |
| 1034.0 | 1036.0 | C | 12.4 | 243. | 0.1 | 220. | 137. | 6.3 | 0.0 | -0.50 | 0.70 |
| 1036.0 | 1038.0 | C | 7.4 | 258. | 0.0 | 217. | 133. | 6.4 | 0.0 | -0.50 | 0.20 |
| 1038.0 | 1039.0 | A | 4.8 | 213. | 0.0 | 219. | 132. | 6.4 | 0.0 | 0.0 | 0.40 |
| 1040.0 | 1041.0 | C | 9.1 | 283. | 0.0 | 224. | 135. | 6.3 | 0.0 | -0.80 | -0.10 |
| 1042.0 | 1043.0 | A | 6.6 | 283. | 0.1 | 223. | 133. | 6.3 | 0.0 | -0.60 | -0.10 |
| 1046.0 | 1048.6 | D | 13.3 | 307. | 0.1 | 208. | 128. | 6.4 | 0.0 | -1.30 | -0.80 |
| 1048.6 | 1050.2 | B | 10.7 | 282. | 0.2 | 206. | 129. | 6.4 | 0.0 | -1.00 | -0.20 |
| 1052.5 | 1054.2 | B | 11.0 | 291. | 0.2 | 212. | 138. | 6.2 | 0.0 | -1.00 | -0.20 |
| 1055.0 | 1056.0 | A | 13.3 | 259. | 0.2 | 239. | 174. | 6.4 | 0.0 | -0.10 | 1.10 |
| 1056.0 | 1058.0 | D | 7.3 | 282. | 0.1 | 249. | 185. | 6.4 | 0.0 | -0.20 | 0.50 |
| 1058.0 | 1059.0 | A | 6.4 | 275. | 0.2 | 249. | 185. | 6.4 | 0.0 | -0.10 | 0.50 |
| 1060.0 | 1062.0 | C | 8.7 | 277. | 0.2 | 251. | 189. | 6.4 | 0.0 | -0.10 | 0.70 |
| 1062.0 | 1064.0 | C | 6.0 | 304. | 0.1 | 255. | 193. | 6.5 | 0.0 | -0.30 | 0.30 |
| 1064.0 | 1065.3 | A | 9.9 | 270. | 0.0 | 257. | 195. | 6.5 | 0.0 | 0.10 | 0.90 |
| 1065.3 | 1066.0 | A | 7.1 | 251. | 0.0 | 258. | 195. | 6.5 | 0.0 | 0.30 | 0.70 |
| 1066.0 | 1067.0 | A | 8.7 | 284. | 0.1 | 259. | 196. | 6.5 | 0.0 | -0.10 | 0.70 |
| 1067.0 | 1068.0 | C | 4.1 | 263. | 0.1 | 261. | 196. | 6.5 | 0.0 | 0.10 | 0.40 |
| 1069.5 | 1070.2 | C | 11.8 | 310. | 0.1 | 268. | 193. | 6.6 | 0.0 | -0.70 | 0.50 |
| 1073.5 | 1074.2 | A | 14.9 | 259. | 0.1 | 285. | 202. | 6.5 | 0.0 | 0.60 | 1.50 |
| 1074.2 | 1075.2 | C | 14.0 | 256. | 0.1 | 288. | 201. | 6.5 | 0.0 | 0.60 | 1.40 |
| 1075.2 | 1076.0 | C | 10.3 | 237. | 0.1 | 291. | 200. | 6.5 | 0.0 | 0.70 | 1.00 |
| 1076.0 | 1077.2 | C | 13.1 | 255. | 0.1 | 292. | 197. | 6.5 | 0.0 | 0.50 | 1.30 |
| 1077.2 | 1078.0 | A | 14.1 | 255. | 0.1 | 292. | 195. | 6.5 | 0.0 | 0.50 | 1.40 |
| 1078.0 | 1079.0 | C | 11.5 | 276. | 0.1 | 293. | 195. | 6.5 | 0.0 | 0.0 | 1.00 |
| 1079.0 | 1081.2 | C | 13.2 | 273. | 0.2 | 296. | 197. | 6.5 | 0.0 | 0.10 | 1.20 |
| 1081.2 | 1082.5 | B | 18.2 | 263. | 0.2 | 297. | 198. | 6.5 | 0.0 | 0.50 | 1.80 |
| 1082.5 | 1084.0 | B | 9.2 | 253. | 0.2 | 305. | 207. | 6.4 | 0.0 | 0.50 | 0.90 |
| 1085.5 | 1086.6 | A | 16.4 | 274. | 0.2 | 283. | 197. | 6.5 | 0.0 | 0.10 | 1.50 |
| 1086.6 | 1088.0 | A | 10.4 | 282. | 0.1 | 284. | 201. | 6.5 | 0.0 | 0.0 | 0.90 |
| 1088.0 | 1090.0 | C | 10.4 | 270. | 0.1 | 272. | 206. | 6.4 | 0.0 | 0.30 | 1.00 |
| 1090.0 | 1091.0 | B | 10.4 | 278. | 0.1 | 271. | 214. | 6.4 | 0.0 | 0.30 | 1.00 |
| 1091.0 | 1092.0 | A | 13.2 | 286. | 0.1 | 294. | 228. | 6.4 | 0.0 | 0.50 | 1.30 |
| 1092.0 | 1094.0 | C | 10.4 | 282. | 0.1 | 317. | 244. | 6.4 | 0.0 | 0.70 | 1.00 |
| 1094.0 | 1095.0 | C | 11.1 | 333. | 0.1 | 330. | 257. | 6.4 | 0.0 | 0.10 | 1.00 |
| 1097.0 | 1098.0 | C | 11.3 | 280. | 0.1 | 338. | 281. | 6.4 | 0.0 | 1.10 | 0.70 |

| CORRELATION INTERVAL | | CORR. GRADE | DIP ANGLE | DIP AZ. | DRFT ANGLE | DRFT AZ. | DIA NO.1 | DIA 13 | DISPLACEMENTS NO.1 | NO.2 | NO.3 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 1098.0 | 1099.6 | D | 9.4 | 271. | 0.0 | 8. | 291. | 6.4 | 0.0 | 0.90 | 0.30 |
| 1100.0 | 1102.0 | A | 8.3 | 288. | 0.0 | 14. | 305. | 6.4 | 0.0 | 0.80 | 0.30 |
| 1102.0 | 1103.0 | B | 10.1 | 280. | 0.0 | 17. | 313. | 6.4 | 0.0 | 0.90 | 0.10 |
| 1103.0 | 1104.0 | B | 8.9 | 272. | 0.0 | 18. | 318. | 6.4 | 0.0 | 0.70 | -0.10 |
| 1104.0 | 1106.0 | D | 11.8 | 289. | 0.0 | 18. | 328. | 6.4 | 0.0 | 1.00 | 0.0 |
| 1106.0 | 1107.0 | A | 7.9 | 306. | 0.0 | 19. | 337. | 6.3 | 0.0 | 0.70 | 0.10 |
| 1107.7 | 1109.0 | B | 8.4 | 282. | 0.0 | 22. | 343. | 6.3 | 0.0 | 0.50 | -0.30 |
| 1109.0 | 1110.2 | B | 10.6 | 274. | 0.0 | 26. | 343. | 6.2 | 0.0 | 0.50 | -0.50 |
| 1112.0 | 1113.0 | C | 12.7 | 293. | 0.0 | 31. | 18. | 6.4 | 0.0 | 0.30 | -0.90 |
| 1114.0 | 1116.0 | C | 11.2 | 292. | 0.0 | 31. | 36. | 6.4 | 0.0 | -0.10 | -1.00 |
| 1116.0 | 1118.0 | C | 12.7 | 303. | 0.1 | 33. | 56. | 6.4 | 0.0 | -0.30 | -1.20 |
| 1118.0 | 1118.8 | C | 11.7 | 284. | 0.2 | 37. | 68. | 6.4 | 0.0 | -0.80 | -1.10 |
| 1118.8 | 1120.0 | C | 12.8 | 291. | 0.2 | 39. | 77. | 6.4 | 0.0 | -0.90 | -1.20 |
| 1120.0 | 1122.0 | D | 12.7 | 287. | 0.2 | 42. | 91. | 6.3 | 0.0 | -1.10 | -1.00 |
| 1122.0 | 1123.5 | C | 15.5 | 304. | 0.2 | 46. | 104. | 6.3 | 0.0 | -1.30 | -1.30 |
| 1123.5 | 1126.5 | A | 15.3 | 296. | 0.1 | 53. | 119. | 6.4 | 0.0 | -1.50 | -0.90 |
| 1126.5 | 1128.0 | D | 15.5 | 285. | 0.1 | 59. | 125. | 6.4 | 0.0 | -1.50 | -0.50 |
| 1128.0 | 1129.5 | C | 17.9 | 281. | 0.1 | 61. | 127. | 6.4 | 0.0 | -1.70 | -0.40 |
| 1132.0 | 1134.0 | D | 18.5 | 333. | 0.0 | 68. | 126. | 6.4 | 0.0 | -1.50 | -1.70 |
| 1144.0 | 1146.2 | D | 15.5 | 6. | 0.0 | 76. | 101. | 6.5 | 0.0 | 0.10 | -1.30 |
| 1152.0 | 1154.0 | B | 11.3 | 223. | 0.0 | 67. | 97. | 6.6 | 0.0 | -0.80 | 0.30 |
| 1171.2 | 1172.0 | D | 7.4 | 311. | 0.0 | 48. | 94. | 6.4 | 0.0 | -0.50 | -0.70 |
| 1176.0 | 1178.0 | D | 9.8 | 238. | 0.1 | 53. | 109. | 6.4 | 0.0 | -0.70 | 0.20 |
| 1184.5 | 1185.5 | C | 34.3 | 246. | 0.1 | 33. | 100. | 6.4 | 0.0 | -3.40 | -0.30 |
| 1190.0 | 1191.0 | C | 13.2 | 294. | 0.0 | 19. | 120. | 6.4 | 0.0 | -1.30 | -0.70 |
| 1192.0 | 1193.0 | C | 22.4 | 270. | 0.1 | 24. | 129. | 6.5 | 0.0 | -2.00 | 0.0 |
| 1197.0 | 1198.2 | C | 8.2 | 269. | 0.0 | 41. | 128. | 6.5 | 0.0 | -0.70 | 0.0 |
| 1198.2 | 1199.5 | C | 7.7 | 276. | 0.0 | 41. | 127. | 6.5 | 0.0 | -0.70 | -0.10 |
| 1200.0 | 1202.0 | C | 8.8 | 259. | 0.0 | 37. | 125. | 6.5 | 0.0 | -0.70 | 0.10 |
| 1204.0 | 1206.0 | C | 12.8 | 244. | 0.0 | 33. | 130. | 6.6 | 0.0 | -0.70 | 0.60 |
| 1206.0 | 1207.2 | B | 10.1 | 249. | 0.0 | 33. | 131. | 6.5 | 0.0 | -0.60 | 0.40 |
| 1207.2 | 1208.5 | A | 6.2 | 255. | 0.0 | 35. | 133. | 6.5 | 0.0 | -0.40 | 0.20 |
| 1208.5 | 1209.2 | A | 8.2 | 251. | 0.0 | 34. | 132. | 6.5 | 0.0 | -0.50 | 0.30 |
| 1217.0 | 1217.5 | A | 13.3 | 290. | 0.0 | 23. | 127. | 6.4 | 0.0 | -1.30 | -0.50 |
| 1217.5 | 1218.6 | B | 15.7 | 280. | 0.0 | 24. | 128. | 6.5 | 0.0 | -1.50 | -0.30 |
| 1218.6 | 1221.0 | C | 11.1 | 280. | 0.0 | 27. | 134. | 6.5 | 0.0 | -1.00 | -0.10 |
| 1221.0 | 1222.0 | D | 8.8 | 265. | 0.0 | 23. | 131. | 6.5 | 0.0 | -0.70 | 0.10 |
| 1223.0 | 1224.2 | C | 8.3 | 279. | 0.0 | 27. | 138. | 6.4 | 0.0 | -0.70 | 0.0 |
| 1224.2 | 1226.0 | C | 12.5 | 262. | 0.0 | 25. | 135. | 6.5 | 0.0 | -0.90 | 0.30 |
| 1226.0 | 1228.0 | D | 13.6 | 268. | 0.0 | 24. | 140. | 6.5 | 0.0 | -1.00 | 0.30 |
| 1228.0 | 1229.7 | C | 16.8 | 277. | 0.0 | 25. | 146. | 6.5 | 0.0 | -1.30 | 0.30 |
| 1230.0 | 1231.5 | A | 13.2 | 253. | 0.0 | 25. | 145. | 6.4 | 0.0 | -0.60 | 0.70 |
| 1232.0 | 1234.2 | C | 13.2 | 257. | 0.0 | 27. | 143. | 6.4 | 0.0 | -0.70 | 0.60 |
| 1234.2 | 1235.0 | C | 17.5 | 264. | 0.0 | 26. | 136. | 6.5 | 0.0 | -1.30 | 0.40 |
| 1236.0 | 1236.5 | A | 13.1 | 247. | 0.0 | 21. | 128. | 6.5 | 0.0 | -0.80 | 0.50 |
| 1238.0 | 1239.0 | A | 13.1 | 231. | 0.0 | 20. | 128. | 6.5 | 0.0 | -0.50 | 0.80 |
| 1240.0 | 1242.0 | C | 17.9 | 251. | 0.0 | 19. | 133. | 6.5 | 0.0 | -1.10 | 0.70 |
| 1242.0 | 1244.0 | D | 14.0 | 251. | 0.0 | 19. | 135. | 6.5 | 0.0 | -0.80 | 0.60 |
| 1244.0 | 1246.0 | C | 15.2 | 256. | 0.0 | 20. | 134. | 6.5 | 0.0 | -1.00 | 0.50 |
| 1246.0 | 1247.0 | D | 16.0 | 254. | 0.0 | 23. | 135. | 6.5 | 0.0 | -1.00 | 0.60 |
| 1248.0 | 1249.0 | A | 13.6 | 224. | 0.1 | 28. | 125. | 6.4 | 0.0 | -0.40 | 0.90 |
| 1255.0 | 1256.0 | A | 13.4 | 227. | 0.3 | 30. | 35. | 6.4 | 0.0 | -1.20 | -1.00 |
| 1256.0 | 1258.0 | C | 15.5 | 215. | 0.4 | 26. | 14. | 6.4 | 0.0 | -1.30 | -1.30 |
| 1260.0 | 1262.0 | B | 24.6 | 241. | 0.5 | 18. | 4. | 6.5 | 0.0 | -1.00 | -2.50 |
| 1262.0 | 1264.0 | A | 21.1 | 219. | 0.5 | 17. | 356. | 6.5 | 0.0 | -1.30 | -2.10 |

| CORRELATION INTERVAL | | CORR. GRADE | DIP ANGLE | DIP AZ. | DRFT ANGLE | DRFT AZ. | DIA NO.1 | DIA 13 | DISPLACEMENTS NO.1 | NO.2 | NO.3 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 1264.0 | 1266.0 | A | 25.3 | 231. | 0.5 | 17. | 3. | 6.5 | 0.0 | -1.40 | -2.60 |
| 1266.0 | 1268.0 | C | 20.1 | 234. | 0.6 | 14. | 4. | 6.5 | 0.0 | -1.00 | -2.00 |
| 1268.0 | 1270.0 | B | 18.6 | 220. | 0.5 | 12. | 356. | 6.4 | 0.0 | -1.10 | -1.80 |
| 1270.0 | 1272.0 | C | 12.8 | 237. | 0.4 | 13. | 356. | 6.4 | 0.0 | -0.40 | -1.20 |
| 1272.0 | 1274.0 | B | 14.6 | 230. | 0.4 | 14. | 4. | 6.4 | 0.0 | -0.80 | -1.40 |
| 1274.0 | 1276.0 | B | 27.0 | 232. | 0.4 | 16. | 8. | 6.5 | 0.0 | -1.70 | -2.80 |
| 1276.0 | 1278.0 | B | 23.1 | 228. | 0.4 | 16. | 10. | 6.5 | 0.0 | -1.60 | -2.30 |
| 1278.0 | 1280.0 | A | 20.0 | 220. | 0.4 | 17. | 8. | 6.5 | 0.0 | -1.50 | -1.90 |
| 1280.0 | 1282.0 | A | 17.3 | 232. | 0.4 | 17. | 7. | 6.5 | 0.0 | -1.00 | -1.70 |
| 1282.0 | 1284.0 | B | 19.1 | 238. | 0.4 | 19. | 13. | 6.5 | 0.0 | -1.10 | -1.90 |
| 1284.0 | 1286.0 | B | 21.2 | 245. | 0.4 | 17. | 19. | 6.4 | 0.0 | -1.20 | -2.10 |
| 1286.0 | 1288.0 | B | 17.9 | 229. | 0.5 | 15. | 22. | 6.4 | 0.0 | -1.40 | -1.60 |
| 1288.0 | 1290.0 | B | 23.1 | 225. | 0.5 | 14. | 24. | 6.4 | 0.0 | -2.00 | -2.00 |
| 1290.0 | 1292.0 | A | 24.5 | 241. | 0.5 | 13. | 24. | 6.4 | 0.0 | -1.70 | -2.40 |
| 1292.0 | 1294.0 | B | 26.6 | 246. | 0.5 | 12. | 24. | 6.4 | 0.0 | -1.70 | -2.70 |
| 1294.0 | 1296.0 | B | 18.3 | 235. | 0.5 | 12. | 25. | 6.5 | 0.0 | -1.40 | -1.70 |
| 1296.0 | 1298.0 | B | 19.2 | 229. | 0.5 | 12. | 25. | 6.5 | 0.0 | -1.60 | -1.70 |
| 1298.0 | 1300.0 | B | 21.0 | 246. | 0.5 | 11. | 24. | 6.5 | 0.0 | -1.30 | -2.10 |
| 1300.0 | 1302.0 | A | 12.2 | 237. | 0.5 | 11. | 27. | 6.5 | 0.0 | -0.90 | -1.10 |
| 1302.0 | 1304.0 | B | 21.8 | 228. | 0.5 | 11. | 27. | 6.5 | 0.0 | -1.90 | -1.90 |
| 1304.0 | 1306.0 | A | 13.9 | 243. | 0.5 | 11. | 26. | 6.4 | 0.0 | -0.90 | -1.30 |
| 1306.0 | 1308.0 | B | 17.7 | 203. | 0.6 | 11. | 26. | 6.4 | 0.0 | -1.70 | -1.00 |
| 1308.0 | 1310.0 | B | 17.4 | 223. | 0.6 | 11. | 26. | 6.4 | 0.0 | -1.50 | -1.40 |
| 1310.0 | 1312.0 | B | 13.9 | 225. | 0.6 | 9. | 29. | 6.5 | 0.0 | -1.20 | -1.10 |
| 1312.0 | 1314.0 | A | 19.1 | 223. | 0.6 | 7. | 35. | 6.5 | 0.0 | -1.80 | -1.40 |
| 1314.0 | 1316.0 | A | 11.6 | 253. | 0.5 | 7. | 49. | 6.4 | 0.0 | -0.90 | -1.00 |
| 1316.0 | 1318.0 | B | 11.7 | 240. | 0.5 | 8. | 67. | 6.4 | 0.0 | -1.10 | -0.60 |
| 1318.0 | 1320.0 | B | 16.5 | 241. | 0.5 | 7. | 71. | 6.4 | 0.0 | -1.60 | -0.80 |
| 1320.0 | 1322.0 | B | 15.4 | 279. | 0.5 | 6. | 72. | 6.4 | 0.0 | -1.20 | -1.40 |
| 1322.0 | 1324.0 | B | 15.5 | 251. | 0.5 | 7. | 79. | 6.4 | 0.0 | -1.50 | -0.80 |
| 1324.0 | 1326.0 | A | 14.8 | 271. | 0.5 | 7. | 88. | 6.4 | 0.0 | -1.40 | -1.00 |
| 1326.0 | 1328.0 | A | 13.9 | 280. | 0.5 | 6. | 94. | 6.4 | 0.0 | -1.30 | -1.00 |
| 1328.0 | 1330.0 | B | 6.0 | 293. | 0.5 | 7. | 97. | 6.4 | 0.0 | -0.50 | -0.50 |
| 1330.0 | 1332.0 | B | 12.4 | 276. | 0.5 | 6. | 102. | 6.4 | 0.0 | -1.20 | -0.70 |
| 1332.0 | 1334.0 | B | 13.4 | 305. | 0.6 | 4. | 111. | 6.4 | 0.0 | -1.20 | -1.10 |
| 1334.0 | 1336.0 | B | 7.9 | 316. | 0.7 | 5. | 120. | 6.5 | 0.0 | -0.70 | -0.70 |
| 1336.0 | 1338.0 | B | 9.9 | 262. | 0.8 | 6. | 125. | 6.4 | 0.0 | -0.80 | 0.0 |
| 1338.0 | 1340.0 | B | 8.2 | 292. | 0.8 | 5. | 127. | 6.4 | 0.0 | -0.80 | -0.40 |
| 1340.0 | 1342.0 | C | 14.0 | 234. | 0.8 | 5. | 132. | 6.4 | 0.0 | -0.50 | 0.80 |
| 1342.0 | 1344.0 | B | 8.8 | 251. | 0.8 | 5. | 144. | 6.4 | 0.0 | -0.40 | 0.40 |
| 1344.0 | 1346.0 | B | 8.1 | 330. | 0.8 | 5. | 147. | 6.4 | 0.0 | -0.80 | -0.60 |
| 1346.0 | 1348.0 | A | 19.2 | 304. | 0.8 | 5. | 147. | 6.4 | 0.0 | -1.90 | -0.60 |
| 1348.0 | 1350.0 | B | 5.5 | 7. | 0.8 | 5. | 149. | 6.4 | 0.0 | -0.40 | -0.60 |
| 1350.0 | 1352.0 | B | 14.2 | 244. | 0.9 | 5. | 148. | 6.4 | 0.0 | -0.40 | 0.90 |
| 1352.0 | 1354.0 | B | 17.4 | 243. | 0.9 | 5. | 150. | 6.4 | 0.0 | -0.40 | 1.20 |
| 1354.0 | 1356.0 | B | 15.4 | 236. | 0.9 | 6. | 153. | 6.4 | 0.0 | -0.10 | 1.20 |
| 1356.0 | 1358.0 | A | 17.7 | 238. | 1.0 | 6. | 155. | 6.4 | 0.0 | -0.10 | 1.40 |
| 1358.0 | 1360.0 | B | 17.4 | 225. | 1.1 | 5. | 152. | 6.4 | 0.0 | 0.20 | 1.50 |
| 1360.0 | 1362.0 | B | 11.3 | 245. | 1.1 | 6. | 151. | 6.4 | 0.0 | -0.30 | 0.70 |
| 1362.0 | 1364.0 | A | 16.8 | 255. | 1.1 | 5. | 151. | 6.4 | 0.0 | -0.70 | 0.90 |
| 1364.0 | 1366.0 | A | 15.0 | 252. | 1.1 | 6. | 149. | 6.4 | 0.0 | -0.60 | 0.80 |
| 1366.0 | 1368.0 | A | 13.3 | 248. | 1.1 | 8. | 151. | 6.4 | 0.0 | -0.40 | 0.80 |
| 1368.0 | 1370.0 | A | 15.7 | 245. | 1.0 | 10. | 154. | 6.4 | 0.0 | -0.30 | 1.10 |
| 1370.0 | 1372.0 | B | 13.2 | 250. | 1.0 | 9. | 153. | 6.4 | 0.0 | -0.40 | 0.80 |
| 1372.0 | 1374.0 | A | 14.0 | 253. | 1.0 | 8. | 152. | 6.4 | 0.0 | -0.50 | 0.80 |

| CORRELATION INTERVAL | | CORR. GRADE | DIP ANGLE | DIP AZ. | DRFT ANGLE | DRFT AZ. | DIA NO.1 | DIA 13 | DISPLACEMENTS NO.1 | NO.2 | NO.3 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 1374.0 | 1376.0 | B | 21.5 | 244. | 1.1 | 8. | 151. | 6.4 | 0.0 | -0.50 | 1.50 |
| 1376.0 | 1378.0 | B | 29.8 | 250. | 1.2 | 7. | 151. | 6.4 | 0.0 | -1.00 | 2.00 |
| 1378.0 | 1380.0 | B | 34.5 | 239. | 1.2 | 7. | 151. | 6.4 | 0.0 | -0.50 | 2.90 |
| 1380.0 | 1382.0 | B | 9.9 | 260. | 1.2 | 7. | 151. | 6.4 | 0.0 | -0.50 | 0.40 |
| 1382.0 | 1384.0 | B | 8.8 | 319. | 1.1 | 7. | 151. | 6.4 | 0.0 | -0.90 | -0.50 |
| 1384.0 | 1386.0 | B | 2.7 | 267. | 1.2 | 7. | 152. | 6.5 | 0.0 | -0.20 | 0.0 |
| 1386.0 | 1388.0 | C | 3.4 | 232. | 1.2 | 9. | 162. | 6.5 | 0.0 | 0.0 | 0.20 |
| 1388.0 | 1390.0 | B | 5.5 | 273. | 1.1 | 10. | 166. | 6.5 | 0.0 | -0.30 | 0.20 |
| 1390.0 | 1392.0 | B | 14.4 | 310. | 1.1 | 7. | 161. | 6.5 | 0.0 | -1.40 | -0.30 |
| 1392.0 | 1394.0 | B | 15.1 | 299. | 1.1 | 8. | 162. | 6.4 | 0.0 | -1.30 | 0.0 |
| 1394.0 | 1396.0 | B | 5.8 | 322. | 1.1 | 10. | 171. | 6.4 | 0.0 | -0.60 | -0.20 |
| 1396.0 | 1398.0 | B | 19.7 | 270. | 1.2 | 9. | 171. | 6.4 | 0.0 | -0.70 | 1.20 |
| 1398.0 | 1400.0 | C | 14.5 | 358. | 1.3 | 8. | 174. | 6.4 | 0.0 | -1.50 | -1.10 |
| 1400.0 | 1402.0 | B | 19.8 | 297. | 1.4 | 7. | 187. | 6.4 | 0.0 | -1.10 | 0.90 |
| 1402.0 | 1404.0 | C | 10.2 | 264. | 1.5 | 8. | 210. | 6.4 | 0.0 | 0.30 | 0.90 |
| 1404.0 | 1406.0 | C | 21.9 | 322. | 1.7 | 9. | 235. | 6.5 | 0.0 | -0.40 | 1.80 |
| 1406.0 | 1408.0 | C | 21.1 | 346. | 1.7 | 12. | 260. | 6.4 | 0.0 | -0.30 | 1.80 |
| 1408.5 | 1410.0 | D | 8.7 | 293. | 1.7 | 12. | 269. | 6.4 | 0.0 | 0.60 | 0.80 |
| 1412.0 | 1414.0 | C | 12.6 | 357. | 1.7 | 13. | 280. | 6.4 | 0.0 | 0.0 | 1.20 |
| 1414.4 | 1416.0 | B | 16.2 | 287. | 1.6 | 15. | 275. | 6.4 | 0.0 | 1.40 | 1.30 |
| 1416.0 | 1418.0 | B | 14.4 | 273. | 1.6 | 14. | 270. | 6.5 | 0.0 | 1.30 | 1.00 |
| 1418.0 | 1420.0 | C | 15.3 | 328. | 1.7 | 14. | 270. | 6.6 | 0.0 | 0.50 | 1.60 |
| 1420.0 | 1422.0 | B | 19.2 | 294. | 1.7 | 13. | 263. | 6.6 | 0.0 | 1.40 | 1.90 |
| 1422.0 | 1424.0 | B | 18.6 | 297. | 1.8 | 11. | 269. | 6.5 | 0.0 | 1.40 | 1.80 |
| 1424.0 | 1426.0 | B | 18.1 | 304. | 1.8 | 11. | 295. | 6.5 | 0.0 | 1.70 | 1.50 |
| 1426.0 | 1428.0 | A | 16.7 | 287. | 1.8 | 14. | 314. | 6.5 | 0.0 | 1.60 | 0.50 |
| 1428.0 | 1430.0 | A | 18.1 | 293. | 1.7 | 16. | 321. | 6.3 | 0.0 | 1.70 | 0.50 |
| 1430.0 | 1432.0 | B | 23.5 | 299. | 1.8 | 15. | 325. | 6.3 | 0.0 | 2.30 | 0.70 |
| 1432.0 | 1434.0 | B | 12.0 | 310. | 1.9 | 14. | 333. | 6.4 | 0.0 | 1.20 | 0.50 |
| 1434.0 | 1436.0 | B | 11.7 | 278. | 1.8 | 15. | 336. | 6.3 | 0.0 | 0.80 | -0.20 |
| 1438.5 | 1440.0 | B | 34.8 | 279. | 1.7 | 15. | 348. | 6.5 | 0.0 | 2.00 | -1.80 |
| 1442.0 | 1444.0 | B | 13.7 | 229. | 1.7 | 17. | 0. | 6.5 | 0.0 | -0.60 | -1.20 |
| 1444.0 | 1446.0 | B | 19.1 | 171. | 1.7 | 17. | 0. | 6.4 | 0.0 | -1.80 | -0.80 |
| 1446.0 | 1448.0 | B | 17.6 | 187. | 1.7 | 18. | 1. | 6.5 | 0.0 | -1.60 | -1.10 |
| 1448.0 | 1450.0 | C | 21.9 | 275. | 1.6 | 19. | 1. | 6.5 | 0.0 | 0.60 | -1.50 |
| 1451.0 | 1452.0 | C | 17.4 | 262. | 1.5 | 16. | 12. | 6.4 | 0.0 | -0.20 | -1.50 |
| 1452.0 | 1454.0 | B | 19.7 | 275. | 1.5 | 16. | 27. | 6.5 | 0.0 | -0.30 | -1.80 |
| 1457.0 | 1458.0 | C | 9.0 | 175. | 1.5 | 12. | 57. | 6.7 | 0.0 | -0.40 | 0.40 |
| 1462.0 | 1464.0 | C | 20.0 | 290. | 1.4 | 14. | 56. | 6.5 | 0.0 | -0.80 | -2.00 |
| 1464.0 | 1466.0 | C | 33.0 | 300. | 1.4 | 16. | 55. | 6.7 | 0.0 | -0.90 | -3.60 |
| 1466.0 | 1468.0 | C | 23.6 | 291. | 1.4 | 16. | 47. | 6.7 | 0.0 | -0.60 | -2.40 |
| 1474.5 | 1476.0 | B | 22.1 | 246. | 1.5 | 15. | 44. | 6.5 | 0.0 | -1.80 | -1.90 |
| 1476.0 | 1478.0 | B | 16.8 | 269. | 1.5 | 13. | 50. | 6.5 | 0.0 | -1.00 | -1.60 |
| 1478.0 | 1480.0 | B | 19.7 | 304. | 1.5 | 14. | 64. | 6.6 | 0.0 | -0.60 | -2.00 |
| 1480.0 | 1482.0 | B | 15.6 | 300. | 1.6 | 15. | 67. | 6.7 | 0.0 | -0.60 | -1.60 |
| 1482.0 | 1484.0 | B | 8.6 | 231. | 1.7 | 14. | 59. | 6.6 | 0.0 | -0.70 | -0.40 |
| 1484.0 | 1486.0 | C | 7.7 | 320. | 1.7 | 13. | 56. | 6.6 | 0.0 | 0.20 | -0.60 |
| 1486.0 | 1488.0 | C | 20.3 | 165. | 1.7 | 15. | 50. | 6.6 | 0.0 | -1.00 | 1.00 |
| 1488.0 | 1490.0 | B | 29.2 | 138. | 1.7 | 15. | 42. | 6.8 | 0.0 | -0.70 | 2.40 |
| 1490.0 | 1492.0 | B | 12.4 | 159. | 1.7 | 12. | 41. | 6.8 | 0.0 | -0.60 | 0.60 |
| 1492.5 | 1494.0 | D | 19.9 | 281. | 1.7 | 12. | 51. | 6.6 | 0.0 | -0.90 | -2.00 |
| 1496.0 | 1498.0 | B | 12.0 | 266. | 1.7 | 12. | 67. | 6.5 | 0.0 | -0.90 | -1.00 |
| 1498.0 | 1500.0 | B | 8.7 | 248. | 1.7 | 13. | 70. | 6.5 | 0.0 | -0.70 | -0.50 |
| 1500.0 | 1502.0 | B | 5.5 | 241. | 1.6 | 12. | 64. | 6.7 | 0.0 | -0.40 | -0.30 |
| 1502.0 | 1504.0 | C | 8.2 | 266. | 1.6 | 11. | 67. | 6.8 | 0.0 | -0.60 | -0.70 |

| CORRELATION INTERVAL | | CORR. GRADE | DIP ANGLE | DIP AZ. | DRFT ANGLE | DRFT AZ. | DIA NO.1 | DIA 13 | DISPLACEMENTS NO.1 | NO.2 | NO.3 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 1504.0 | 1506.0 | C | 7.9 | 279. | 1.6 | 13. | 82. | 6.8 | 0.0 | -0.60 | -0.70 |
| 1508.0 | 1510.0 | C | 5.3 | 245. | 1.7 | 14. | 87. | 6.7 | 0.0 | -0.40 | -0.20 |
| 1512.0 | 1514.0 | C | 13.3 | 335. | 1.7 | 13. | 87. | 6.9 | 0.0 | -0.20 | -1.40 |
| 1514.0 | 1516.0 | C | 12.1 | 295. | 1.7 | 12. | 88. | 6.8 | 0.0 | -0.90 | -1.20 |
| 1516.0 | 1518.0 | C | 12.2 | 289. | 1.7 | 13. | 91. | 6.7 | 0.0 | -1.00 | -1.10 |
| 1526.0 | 1528.0 | C | 20.7 | 223. | 1.9 | 17. | 44. | 6.5 | 0.0 | -1.90 | -1.20 |
| 1530.0 | 1532.0 | C | 24.4 | 266. | 1.7 | 15. | 46. | 6.5 | 0.0 | -1.50 | -2.40 |
| 1532.0 | 1534.0 | C | 28.5 | 335. | 1.6 | 14. | 69. | 6.7 | 0.0 | 0.40 | -2.60 |
| 1534.0 | 1536.0 | C | 36.1 | 327. | 1.6 | 14. | 91. | 6.7 | 0.0 | -1.70 | -4.30 |
| 1536.0 | 1538.0 | C | 31.7 | 323. | 1.6 | 15. | 97. | 6.8 | 0.0 | -2.00 | -3.70 |
| 1538.0 | 1540.0 | C | 25.7 | 325. | 1.6 | 17. | 101. | 6.8 | 0.0 | -1.60 | -2.90 |
| 1542.5 | 1544.5 | C | 40.7 | 286. | 1.6 | 17. | 99. | 6.9 | 0.0 | -4.80 | -3.70 |
| 1546.0 | 1548.0 | C | 29.2 | 347. | 1.7 | 17. | 95. | 6.9 | 0.0 | -0.40 | -3.20 |
| 1549.5 | 1550.6 | C | 21.5 | 42. | 1.6 | 19. | 107. | 6.8 | 0.0 | 1.40 | -1.10 |
| 1554.0 | 1555.1 | C | 11.8 | 85. | 1.6 | 19. | 96. | 6.8 | 0.0 | 7.80 | 3.60 |
| 1558.0 | 1560.0 | C | 23.3 | 330. | 1.6 | 19. | 97. | 6.8 | 0.0 | -1.10 | -2.60 |
| 1566.0 | 1568.0 | C | 26.8 | 321. | 1.6 | 21. | 105. | 6.7 | 0.0 | -2.00 | -2.90 |
| 1568.0 | 1570.0 | C | 11.7 | 275. | 1.7 | 20. | 99. | 6.8 | 0.0 | -2.20 | -1.40 |
| 1570.0 | 1572.0 | C | 15.3 | 358. | 1.6 | 20. | 94. | 6.8 | 0.0 | 0.20 | -1.40 |
| 1572.0 | 1574.0 | B | 17.0 | 333. | 1.5 | 22. | 96. | 6.7 | 0.0 | -0.60 | -1.80 |
| 1574.0 | 1576.0 | B | 16.6 | 339. | 1.5 | 25. | 102. | 6.8 | 0.0 | -0.60 | -1.80 |
| 1576.0 | 1578.0 | A | 12.8 | 343. | 1.5 | 26. | 108. | 6.8 | 0.0 | -0.50 | -1.40 |
| 1578.0 | 1580.0 | C | 16.6 | 344. | 1.5 | 27. | 103. | 6.8 | 0.0 | -0.20 | -1.70 |
| 1580.0 | 1582.0 | B | 17.3 | 350. | 1.6 | 28. | 102. | 6.8 | 0.0 | -0.30 | -1.80 |
| 1582.0 | 1584.0 | B | 21.8 | 6. | 1.6 | 30. | 101. | 6.8 | 0.0 | 0.30 | -2.00 |
| 1584.0 | 1586.0 | B | 17.3 | 3. | 1.7 | 29. | 100. | 6.8 | 0.0 | 0.20 | -1.60 |
| 1586.0 | 1588.0 | B | 16.6 | 4. | 1.6 | 28. | 100. | 6.7 | 0.0 | 0.20 | -1.50 |
| 1588.0 | 1590.0 | B | 25.7 | 350. | 1.6 | 31. | 92. | 6.7 | 0.0 | 0.0 | -2.50 |
| 1590.0 | 1592.0 | B | 26.3 | 328. | 1.6 | 33. | 92. | 6.8 | 0.0 | -1.10 | -2.90 |
| 1594.0 | 1596.0 | A | 24.7 | 324. | 1.7 | 32. | 103. | 6.8 | 0.0 | -1.60 | -2.70 |
| 1596.0 | 1598.0 | C | 32.0 | 268. | 1.8 | 33. | 110. | 6.8 | 0.0 | -3.40 | -1.10 |
| 1602.0 | 1604.0 | B | 17.1 | 315. | 1.7 | 34. | 95. | 6.5 | 0.0 | -1.00 | -1.70 |
| 1604.5 | 1606.3 | B | 16.8 | 342. | 1.7 | 33. | 109. | 6.7 | 0.0 | -0.70 | -1.80 |
| 1607.0 | 1608.0 | C | 1.3 | 274. | 1.8 | 35. | 109. | 6.8 | 0.0 | 0.0 | -0.10 |
| 1608.0 | 1610.0 | C | 17.0 | 216. | 1.8 | 36. | 111. | 6.8 | 0.0 | -0.60 | 1.00 |
| 1610.0 | 1612.0 | C | 16.7 | 175. | 1.8 | 36. | 102. | 6.7 | 0.0 | 0.40 | 1.60 |
| 1614.5 | 1616.0 | C | 21.5 | 340. | 1.8 | 36. | 71. | 6.6 | 0.0 | 0.50 | -1.70 |
| 1618.5 | 1620.0 | C | 16.8 | 339. | 2.0 | 37. | 94. | 6.7 | 0.0 | -0.30 | -1.70 |
| 1620.5 | 1622.0 | B | 15.5 | 337. | 2.1 | 36. | 101. | 6.6 | 0.0 | -0.50 | -1.60 |
| 1622.0 | 1624.0 | B | 21.5 | 7. | 2.1 | 35. | 98. | 6.6 | 0.0 | 0.50 | -1.80 |
| 1624.0 | 1626.0 | B | 15.6 | 352. | 2.1 | 35. | 97. | 6.7 | 0.0 | 0.0 | -1.50 |
| 1626.0 | 1628.0 | B | 18.4 | 342. | 2.1 | 36. | 93. | 6.6 | 0.0 | -0.20 | -1.80 |
| 1628.0 | 1630.0 | C | 24.6 | 263. | 2.0 | 37. | 83. | 6.7 | 0.0 | -2.40 | -1.60 |
| 1630.0 | 1632.0 | B | 31.0 | 275. | 2.0 | 38. | 85. | 6.6 | 0.0 | -3.00 | -2.50 |
| 1632.0 | 1634.0 | B | 27.7 | 338. | 1.9 | 40. | 90. | 6.5 | 0.0 | -0.50 | -2.80 |
| 1634.0 | 1636.0 | B | 23.4 | 333. | 1.9 | 42. | 95. | 6.5 | 0.0 | -0.80 | -2.40 |
| 1636.0 | 1638.0 | B | 22.8 | 333. | 2.1 | 43. | 101. | 6.6 | 0.0 | -1.00 | -2.40 |
| 1638.0 | 1640.0 | C | 31.4 | 279. | 2.2 | 43. | 100. | 6.6 | 0.0 | -3.20 | -2.10 |
| 1640.0 | 1642.0 | B | 27.3 | 319. | 2.2 | 43. | 100. | 6.7 | 0.0 | -1.80 | -2.90 |
| 1642.0 | 1644.0 | A | 24.9 | 320. | 2.2 | 44. | 104. | 6.7 | 0.0 | -1.70 | -2.60 |
| 1644.0 | 1646.0 | A | 26.3 | 324. | 2.2 | 44. | 104. | 6.7 | 0.0 | -1.70 | -2.80 |
| 1646.0 | 1648.0 | B | 21.2 | 333. | 2.3 | 44. | 99. | 6.6 | 0.0 | -0.80 | -2.20 |
| 1648.0 | 1650.0 | B | 19.1 | 342. | 2.3 | 43. | 99. | 6.5 | 0.0 | -0.40 | -1.90 |
| 1650.0 | 1652.0 | B | 22.4 | 328. | 2.3 | 43. | 104. | 6.5 | 0.0 | -1.20 | -2.30 |
| 1652.0 | 1654.0 | B | 12.2 | 323. | 2.2 | 42. | 102. | 6.5 | 0.0 | -0.60 | -1.20 |

| CORRELATION INTERVAL | | CORR. GRADE | DIP ANGLE | DIP AZ. | DRFT ANGLE | DRFT AZ. | DIA NO.1 | DIA 13 | DISPLACEMENTS NO.1 | NO.2 | NO.3 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 1654.0 | 1656.0 | C | 15.6 | 340. | 2.2 | 42. | 104. | 6.6 | 0.0 | -0.50 | -1.60 |
| 1656.0 | 1658.0 | C | 31.3 | 273. | 2.3 | 43. | 106. | 6.6 | 0.0 | -3.20 | -1.50 |
| 1658.0 | 1660.0 | C | 14.1 | 290. | 2.3 | 42. | 105. | 6.6 | 0.0 | -1.20 | -1.00 |
| 1660.0 | 1662.0 | B | 14.3 | 335. | 2.3 | 43. | 111. | 6.7 | 0.0 | -0.70 | -1.50 |
| 1662.0 | 1664.0 | B | 20.8 | 321. | 2.3 | 43. | 110. | 6.7 | 0.0 | -1.50 | -2.10 |
| 1664.0 | 1666.0 | B | 21.3 | 323. | 2.3 | 41. | 101. | 6.6 | 0.0 | -1.20 | -2.20 |
| 1666.0 | 1668.0 | B | 23.3 | 349. | 2.4 | 43. | 98. | 6.6 | 0.0 | -0.20 | -2.30 |
| 1672.0 | 1674.0 | C | 8.6 | 349. | 2.4 | 50. | 91. | 6.7 | 0.0 | 0.20 | -0.70 |
| 1674.0 | 1676.0 | B | 14.5 | 338. | 2.4 | 49. | 94. | 6.7 | 0.0 | -0.20 | -1.40 |
| 1678.0 | 1680.0 | C | 24.4 | 323. | 2.5 | 53. | 96. | 6.6 | 0.0 | -1.20 | -2.50 |
| 1680.0 | 1682.0 | B | 19.7 | 329. | 2.4 | 51. | 105. | 6.6 | 0.0 | -1.00 | -2.00 |
| 1682.0 | 1684.0 | B | 19.8 | 332. | 2.4 | 49. | 132. | 6.4 | 0.0 | -1.60 | -1.80 |
| 1684.0 | 1686.0 | C | 13.3 | 333. | 2.5 | 49. | 152. | 6.3 | 0.0 | -1.20 | -1.00 |
| 1686.0 | 1688.0 | B | 21.3 | 321. | 2.4 | 46. | 154. | 6.4 | 0.0 | -2.10 | -1.10 |
| 1688.0 | 1690.0 | A | 19.5 | 319. | 2.4 | 47. | 146. | 6.5 | 0.0 | -1.90 | -1.20 |
| 1690.0 | 1692.0 | B | 21.0 | 295. | 2.4 | 50. | 141. | 6.4 | 0.0 | -1.90 | -0.60 |
| 1692.0 | 1694.0 | B | 24.4 | 317. | 2.3 | 52. | 145. | 6.4 | 0.0 | -2.40 | -1.40 |
| 1694.0 | 1696.0 | B | 26.3 | 318. | 2.4 | 53. | 144. | 6.4 | 0.0 | -2.60 | -1.60 |
| 1696.0 | 1698.0 | B | 22.0 | 333. | 2.5 | 52. | 143. | 6.4 | 0.0 | -2.00 | -1.80 |
| 1698.0 | 1700.0 | B | 26.3 | 329. | 2.5 | 51. | 144. | 6.3 | 0.0 | -2.50 | -2.00 |
| 1703.5 | 1704.5 | C | 46.7 | 345. | 2.5 | 53. | 150. | 6.4 | 0.0 | -5.30 | -4.90 |
| 1711.0 | 1712.5 | C | 27.6 | 351. | 2.6 | 48. | 168. | 6.5 | 0.0 | -2.90 | -2.20 |
| 1713.0 | 1715.5 | C | 30.6 | 304. | 2.6 | 51. | 170. | 6.5 | 0.0 | -2.60 | 0.20 |
| 1718.0 | 1720.0 | C | 29.5 | 318. | 2.8 | 50. | 178. | 6.4 | 0.0 | -2.70 | -0.20 |
| 1720.0 | 1722.5 | B | 30.2 | 315. | 2.8 | 51. | 184. | 6.4 | 0.0 | -2.50 | 0.30 |
| 1722.5 | 1724.0 | C | 19.8 | 315. | 2.9 | 54. | 188. | 6.4 | 0.0 | -1.50 | 0.20 |
| 1726.0 | 1728.0 | C | 31.7 | 315. | 2.9 | 56. | 200. | 6.4 | 0.0 | -2.00 | 1.20 |
| 1728.0 | 1730.0 | B | 28.8 | 335. | 2.9 | 53. | 203. | 6.4 | 0.0 | -2.50 | 0.20 |
| 1730.0 | 1732.0 | B | 15.1 | 339. | 2.9 | 50. | 201. | 6.4 | 0.0 | -1.40 | -0.20 |
| 1733.0 | 1735.0 | C | 40.7 | 313. | 2.7 | 56. | 184. | 6.2 | 0.0 | -3.40 | 0.70 |
| 1740.0 | 1742.0 | B | 30.3 | 314. | 2.7 | 55. | 162. | 6.5 | 0.0 | -3.00 | -0.80 |
| 1742.0 | 1744.0 | C | 5.9 | 298. | 2.8 | 56. | 168. | 6.5 | 0.0 | -0.40 | -0.10 |
| 1750.0 | 1752.0 | C | 32.7 | 137. | 3.0 | 54. | 187. | 6.5 | 0.0 | 2.70 | -1.00 |
| 1754.0 | 1755.0 | C | 39.9 | 245. | 3.1 | 55. | 199. | 6.5 | 0.0 | 2.50 | 4.20 |
| 1778.0 | 1780.0 | C | 39.8 | 317. | 3.1 | 52. | 174. | 6.4 | 0.0 | -4.00 | -0.40 |
| 1784.0 | 1785.5 | C | 15.3 | 210. | 3.2 | 53. | 152. | 6.4 | 0.0 | 0.70 | 1.30 |
| 1790.0 | 1792.0 | B | 25.2 | 247. | 3.3 | 55. | 192. | 6.3 | 0.0 | 1.00 | 2.20 |
| 1806.0 | 1808.0 | B | 43.3 | 318. | 3.3 | 55. | 171. | 6.5 | 0.0 | -4.70 | -0.80 |
| 1808.0 | 1810.0 | C | 44.7 | 324. | 3.3 | 54. | 181. | 6.4 | 0.0 | -4.60 | -0.50 |
| 1827.5 | 1828.5 | D | 46.5 | 271. | 3.3 | 55. | 171. | 6.6 | 0.0 | -1.80 | 3.50 |
| 1832.5 | 1834.0 | D | 41.5 | 284. | 3.5 | 53. | 167. | 6.3 | 0.0 | -2.70 | 1.60 |
| 1848.0 | 1850.0 | C | 44.1 | 308. | 3.7 | 58. | 134. | 6.5 | 0.0 | -5.00 | -3.00 |
| 1850.0 | 1852.0 | C | 32.4 | 29. | 3.7 | 56. | 135. | 6.5 | 0.0 | -0.20 | -3.50 |
| 1856.5 | 1858.0 | D | 4.5 | 42. | 3.8 | 56. | 127. | 6.6 | 0.0 | 0.40 | -0.40 |
| 1862.6 | 1863.0 | C | 35.2 | 131. | 3.7 | 53. | 86. | 6.3 | 0.0 | 2.70 | 4.10 |
| 1872.0 | 1874.0 | C | 23.1 | 231. | 3.9 | 54. | 106. | 6.6 | 0.0 | -1.30 | 0.70 |
| 1874.0 | 1876.0 | C | 16.2 | 288. | 3.9 | 54. | 101. | 6.6 | 0.0 | -1.20 | -1.10 |
| 1878.5 | 1880.0 | C | 23.0 | 243. | 3.7 | 56. | 172. | 6.2 | 0.0 | 0.40 | 1.80 |
| 1880.0 | 1882.0 | B | 24.6 | 255. | 3.7 | 55. | 188. | 6.3 | 0.0 | 0.50 | 2.00 |
| 1884.0 | 1886.0 | B | 26.0 | 265. | 3.9 | 51. | 207. | 6.3 | 0.0 | 0.80 | 2.20 |
| 1909.3 | 1912.5 | B | 8.9 | 96. | 3.8 | 51. | 169. | 6.4 | 0.0 | 0.40 | -0.80 |
| 1920.0 | 1921.5 | C | 15.9 | 272. | 3.9 | 46. | 179. | 6.4 | 0.0 | -0.40 | 0.80 |
| 1936.0 | 1938.0 | C | 21.0 | 356. | 3.9 | 47. | 185. | 6.2 | 0.0 | -2.20 | -1.40 |
| 1942.0 | 1944.0 | C | 11.8 | 261. | 4.0 | 50. | 178. | 6.3 | 0.0 | -0.10 | 0.60 |
| 1946.0 | 1948.0 | C | 27.5 | 315. | 3.9 | 49. | 177. | 6.0 | 0.0 | -2.30 | -0.20 |

| CORRELATION INTERVAL | | CORR. GRADE | DIP ANGLE | DIP AZ. | DRFT ANGLE | DRFT AZ. | AZ. NO.1 | DIA 13 | DISPLACEMENTS NO.1 | NO.2 | NO.3 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 1949.0 | 1951.0 | C | 20.1 | 329. | 3.8 | 47. | 170. | 6.1 | 0.0 | -1.90 | -0.90 |
| 1953.0 | 1954.5 | B | 16.1 | 335. | 3.8 | 49. | 158. | 6.3 | 0.0 | -1.50 | -1.20 |
| 1956.0 | 1958.0 | B | 13.3 | 273. | 3.9 | 49. | 153. | 6.3 | 0.0 | -0.70 | 0.20 |
| 1958.0 | 1960.0 | C | 22.4 | 268. | 4.0 | 50. | 149. | 6.3 | 0.0 | -1.20 | 0.60 |
| 1966.0 | 1968.0 | A | 27.2 | 276. | 3.9 | 46. | 158. | 6.4 | 0.0 | -1.60 | 0.80 |
| 1968.0 | 1970.0 | B | 22.7 | 274. | 3.9 | 46. | 156. | 6.4 | 0.0 | -1.30 | 0.60 |
| 1970.0 | 1972.0 | B | 17.9 | 267. | 3.9 | 47. | 156. | 6.4 | 0.0 | -0.80 | 0.60 |
| 1972.0 | 1974.0 | B | 14.4 | 93. | 3.9 | 48. | 157. | 6.4 | 0.0 | 0.90 | -0.90 |
| 1977.0 | 1979.0 | C | 30.9 | 224. | 4.1 | 48. | 165. | 6.3 | 0.0 | 1.20 | 2.80 |
| 1982.0 | 1984.0 | C | 8.6 | 204. | 4.2 | 49. | 174. | 6.2 | 0.0 | 0.60 | 0.40 |
| 1984.0 | 1986.0 | C | 19.2 | 243. | 4.2 | 48. | 176. | 6.2 | 0.0 | 0.40 | 1.40 |
| 1986.0 | 1988.5 | C | 13.7 | 213. | 4.3 | 48. | 172. | 6.1 | 0.0 | 0.80 | 0.90 |
| 1990.0 | 1992.0 | C | 25.0 | 186. | 4.2 | 48. | 161. | 6.2 | 0.0 | 2.10 | 1.90 |
| 1996.0 | 1998.0 | C | 28.2 | 245. | 4.1 | 46. | 146. | 6.1 | 0.0 | -0.70 | 1.60 |
| 2002.3 | 2004.5 | C | 21.1 | 140. | 4.0 | 47. | 143. | 6.1 | 0.0 | 2.20 | 1.00 |
| 2004.5 | 2006.5 | B | 20.9 | 137. | 3.9 | 47. | 134. | 6.1 | 0.0 | 2.20 | 1.20 |
| 2008.0 | 2010.0 | C | 14.0 | 144. | 3.8 | 46. | 149. | 6.0 | 0.0 | 1.40 | 0.50 |
| 2012.0 | 2014.0 | C | 15.2 | 182. | 3.7 | 44. | 157. | 6.0 | 0.0 | 1.20 | 1.00 |
| 2022.0 | 2024.0 | B | 10.7 | 187. | 3.7 | 48. | 172. | 6.2 | 0.0 | 0.90 | 0.50 |
| 2024.0 | 2026.0 | B | 21.8 | 235. | 3.8 | 48. | 172. | 6.1 | 0.0 | 0.60 | 1.70 |
| 2030.0 | 2032.0 | B | 5.3 | 10. | 4.0 | 46. | 163. | 6.4 | 0.0 | -0.40 | -0.80 |
| 2036.0 | 2037.5 | C | 19.3 | 272. | 4.0 | 43. | 157. | 6.2 | 0.0 | -1.00 | 0.50 |
| 2044.0 | 2046.0 | B | 12.5 | 294. | 3.9 | 42. | 146. | 6.3 | 0.0 | -1.00 | -0.40 |
| 2048.0 | 2050.0 | B | 18.6 | 187. | 4.0 | 42. | 141. | 6.4 | 0.0 | 1.20 | 1.60 |
| 2052.0 | 2054.0 | C | 20.1 | 226. | 4.0 | 45. | 148. | 6.4 | 0.0 | 0.20 | 1.50 |
| 2060.0 | 2062.0 | C | 15.9 | 203. | 3.8 | 43. | 149. | 6.4 | 0.0 | 0.80 | 1.30 |
| 2062.0 | 2064.0 | D | 16.9 | 240. | 3.8 | 42. | 149. | 6.4 | 0.0 | -0.20 | 1.00 |
| 2070.0 | 2072.0 | C | 14.2 | 268. | 3.9 | 42. | 147. | 6.4 | 0.0 | -0.80 | 0.20 |
| 2076.0 | 2078.0 | C | 25.9 | 127. | 3.8 | 42. | 157. | 6.2 | 0.0 | 2.50 | 0.10 |
| 2078.0 | 2080.0 | C | 16.2 | 131. | 3.8 | 41. | 162. | 6.0 | 0.0 | 1.40 | -0.10 |
| 2082.0 | 2084.0 | C | 26.9 | 258. | 3.8 | 42. | 166. | 5.9 | 0.0 | -0.50 | 1.60 |
| 2086.0 | 2088.0 | C | 15.5 | 116. | 3.8 | 45. | 178. | 6.0 | 0.0 | 0.80 | -0.90 |
| 2100.0 | 2102.0 | B | 21.2 | 143. | 3.6 | 41. | 191. | 6.4 | 0.0 | 1.50 | -0.70 |
| 2106.0 | 2108.0 | C | 31.1 | 272. | 3.6 | 43. | 167. | 6.1 | 0.0 | -1.30 | 1.50 |
| 2112.0 | 2114.0 | C | 44.5 | 273. | 3.5 | 43. | 179. | 6.1 | 0.0 | -1.20 | 3.30 |
| 2116.0 | 2117.0 | C | 27.4 | 258. | 3.6 | 42. | 189. | 6.1 | 0.0 | 0.40 | 2.20 |
| 2126.5 | 2127.5 | C | 14.9 | 305. | 3.4 | 41. | 185. | 6.1 | 0.0 | -1.00 | 0.20 |
| 2142.3 | 2142.4 | C | 31.4 | 59. | 3.5 | 42. | 192. | 6.3 | 0.0 | -2.10 | -3.80 |
| 2147.0 | 2147.2 | B | 16.7 | 12. | 3.6 | 42. | 188. | 6.4 | 0.0 | -1.80 | -1.50 |
| 2153.6 | 2154.0 | C | 16.0 | 116. | 3.5 | 42. | 191. | 6.5 | 0.0 | 0.50 | -1.30 |
| 2156.0 | 2157.0 | B | 11.5 | 52. | 3.5 | 42. | 186. | 6.5 | 0.0 | -0.80 | -1.50 |
| 2158.0 | 2158.3 | C | 6.0 | 359. | 3.4 | 41. | 180. | 6.5 | 0.0 | -0.70 | -0.70 |
| 2162.0 | 2162.3 | C | 16.4 | 343. | 3.3 | 45. | 189. | 6.4 | 0.0 | -1.70 | -0.70 |
| 2163.0 | 2163.3 | B | 19.2 | 51. | 3.3 | 44. | 189. | 6.5 | 0.0 | -1.40 | -2.30 |
| 2164.0 | 2164.2 | B | 20.7 | 35. | 3.3 | 43. | 188. | 6.5 | 0.0 | -1.90 | -2.30 |
| 2166.0 | 2166.4 | C | 18.8 | 22. | 3.3 | 43. | 173. | 6.5 | 0.0 | -1.60 | -2.10 |
| 2169.8 | 2170.0 | B | 12.6 | 16. | 3.3 | 42. | 161. | 6.5 | 0.0 | -0.90 | -1.50 |
| 2170.6 | 2170.8 | B | 10.6 | 16. | 3.3 | 43. | 158. | 6.5 | 0.0 | -0.70 | -1.30 |
| 2172.0 | 2172.3 | C | 13.2 | 43. | 3.2 | 45. | 153. | 6.5 | 0.0 | -0.20 | -1.50 |
| 2173.6 | 2174.0 | C | 23.1 | 48. | 3.3 | 45. | 155. | 6.4 | 0.0 | -0.30 | -2.50 |
| 2179.6 | 2179.8 | C | 20.4 | 17. | 3.1 | 45. | 156. | 6.4 | 0.0 | -1.30 | -2.30 |
| 2182.0 | 2182.3 | B | 17.6 | 20. | 3.1 | 45. | 155. | 6.4 | 0.0 | -1.00 | -2.00 |
| 2183.2 | 2183.3 | A | 16.7 | 14. | 3.2 | 47. | 156. | 6.5 | 0.0 | -1.10 | -1.90 |
| 2185.0 | 2185.2 | C | 10.2 | 8. | 3.2 | 48. | 156. | 6.5 | 0.0 | -0.70 | -1.20 |
| 2187.6 | 2187.7 | C | 19.5 | 13. | 3.1 | 49. | 163. | 6.4 | 0.0 | -1.50 | -2.10 |

| CORRELATION INTERVAL | | CORR. GRADE | DIP ANGLE | DIP AZ. | DRFT ANGLE | DRFT AZ. | DIA NO.1 | DIA 13 | DISPLACEMENTS NO.1 | NO.2 | NO.3 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 2189.3 | 2189.4 | C | 26.3 | 20. | 3.1 | 49. | 168. | 6.4 | 0.0 | -2.10 | -2.90 |
| 2196.0 | 2196.5 | C | 21.8 | 41. | 3.1 | 48. | 164. | 6.4 | 0.0 | -0.90 | -2.50 |
| 2198.3 | 2198.4 | C | 19.9 | 27. | 3.0 | 47. | 165. | 6.5 | 0.0 | -1.30 | -2.30 |
| 2201.3 | 2201.5 | C | 20.0 | 23. | 3.1 | 48. | 162. | 6.5 | 0.0 | -1.30 | -2.30 |
| 2202.6 | 2203.1 | C | 24.6 | 27. | 3.1 | 48. | 167. | 6.4 | 0.0 | -1.70 | -2.80 |
| 2205.7 | 2205.9 | B | 19.6 | 28. | 3.2 | 48. | 174. | 6.4 | 0.0 | -1.50 | -2.20 |
| 2207.0 | 2207.2 | B | 20.5 | 25. | 3.1 | 48. | 169. | 6.4 | 0.0 | -1.50 | -2.30 |
| 2209.0 | 2209.3 | B | 23.4 | 34. | 3.2 | 50. | 168. | 6.4 | 0.0 | -1.40 | -2.70 |
| 2211.3 | 2211.4 | B | 25.0 | 30. | 3.3 | 52. | 181. | 6.3 | 0.0 | -2.10 | -2.70 |
| 2214.0 | 2214.2 | C | 23.4 | 19. | 3.2 | 51. | 186. | 6.3 | 0.0 | -2.30 | -2.20 |
| 2216.2 | 2216.7 | B | 26.4 | 25. | 3.1 | 49. | 180. | 6.4 | 0.0 | -2.40 | -2.80 |
| 2218.3 | 2218.4 | C | 30.2 | 10. | 3.0 | 50. | 178. | 6.6 | 0.0 | -3.20 | -2.90 |
| 2223.2 | 2223.5 | C | 27.1 | 33. | 3.0 | 52. | 194. | 6.5 | 0.0 | -2.70 | -2.80 |
| 2225.8 | 2226.0 | C | 22.2 | 25. | 2.9 | 54. | 191. | 6.4 | 0.0 | -2.20 | -2.10 |
| 2227.3 | 2228.4 | C | 25.4 | 18. | 2.9 | 54. | 184. | 6.4 | 0.0 | -2.50 | -2.40 |
| 2229.6 | 2230.0 | C | 14.6 | 39. | 2.9 | 52. | 183. | 6.5 | 0.0 | -1.10 | -1.70 |
| 2230.5 | 2230.6 | A | 13.2 | 16. | 2.9 | 53. | 184. | 6.5 | 0.0 | -1.30 | -1.30 |
| 2232.8 | 2232.9 | D | 21.2 | 22. | 2.9 | 55. | 186. | 6.6 | 0.0 | -2.10 | -2.10 |
| 2237.6 | 2237.7 | C | 15.0 | 44. | 2.9 | 55. | 178. | 6.6 | 0.0 | -0.90 | -1.80 |
| 2240.0 | 2240.3 | C | 15.3 | 355. | 2.9 | 55. | 186. | 6.5 | 0.0 | -1.60 | -1.00 |
| 2243.0 | 2243.1 | C | 27.9 | 348. | 2.7 | 54. | 178. | 6.5 | 0.0 | -3.00 | -1.70 |
| 2245.9 | 2246.0 | C | 26.0 | 32. | 2.7 | 54. | 179. | 6.5 | 0.0 | -2.10 | -2.90 |
| 2253.6 | 2253.7 | C | 10.8 | 57. | 2.7 | 57. | 173. | 6.6 | 0.0 | -0.30 | -1.30 |
| 2256.6 | 2256.7 | C | 12.6 | 24. | 2.8 | 55. | 180. | 6.6 | 0.0 | -1.10 | -1.40 |
| 2265.6 | 2266.0 | D | 8.8 | 94. | 2.8 | 61. | 190. | 6.5 | 0.0 | 0.0 | -1.00 |
| 2267.7 | 2267.8 | B | 13.3 | 16. | 2.8 | 62. | 189. | 6.4 | 0.0 | -1.30 | -1.20 |
| 2270.5 | 2270.6 | B | 12.9 | 12. | 2.7 | 58. | 189. | 6.4 | 0.0 | -1.30 | -1.10 |
| 2272.0 | 2272.4 | B | 14.4 | 21. | 2.7 | 58. | 188. | 6.5 | 0.0 | -1.40 | -1.40 |
| 2275.0 | 2275.3 | B | 21.8 | 39. | 2.7 | 58. | 195. | 6.5 | 0.0 | -2.00 | -2.30 |
| 2277.7 | 2277.8 | C | 22.2 | 48. | 2.8 | 58. | 194. | 6.5 | 0.0 | -1.80 | -2.50 |
| 2280.0 | 2280.3 | C | 25.1 | 24. | 2.8 | 58. | 194. | 6.5 | 0.0 | -2.60 | -2.30 |
| 2282.0 | 2282.3 | C | 26.3 | 27. | 2.8 | 58. | 196. | 6.4 | 0.0 | -2.70 | -2.40 |
| 2286.0 | 2286.4 | C | 18.1 | 7. | 2.8 | 61. | 192. | 6.5 | 0.0 | -1.90 | -1.30 |
| 2288.0 | 2288.3 | C | 27.7 | 32. | 2.8 | 64. | 191. | 6.4 | 0.0 | -2.60 | -2.80 |
| 2290.0 | 2290.3 | B | 26.2 | 51. | 2.7 | 61. | 187. | 6.4 | 0.0 | -1.70 | -3.00 |
| 2292.0 | 2292.6 | B | 25.2 | 45. | 2.6 | 60. | 190. | 6.2 | 0.0 | -1.90 | -2.70 |
| 2294.6 | 2295.0 | C | 29.0 | 53. | 2.7 | 61. | 192. | 6.5 | 0.0 | -2.10 | -3.40 |
| 2297.6 | 2298.0 | B | 20.4 | 58. | 2.7 | 62. | 200. | 6.4 | 0.0 | -1.50 | -2.30 |
| 2298.0 | 2298.4 | C | 19.7 | 36. | 2.7 | 62. | 200. | 6.4 | 0.0 | -1.90 | -1.90 |
| 2302.0 | 2302.3 | B | 17.5 | 30. | 2.6 | 60. | 195. | 6.5 | 0.0 | -1.70 | -1.70 |
| 2305.0 | 2305.3 | B | 15.7 | 41. | 2.4 | 62. | 192. | 6.5 | 0.0 | -1.30 | -1.70 |
| 2306.8 | 2307.3 | B | 19.3 | 41. | 2.4 | 65. | 188. | 6.5 | 0.0 | -1.50 | -2.10 |
| 2309.0 | 2309.4 | C | 20.5 | 358. | 2.5 | 67. | 186. | 6.5 | 0.0 | -2.10 | -1.30 |
| 2311.7 | 2312.0 | C | 15.6 | 43. | 2.6 | 67. | 191. | 6.4 | 0.0 | -1.20 | -1.70 |
| 2312.0 | 2312.8 | B | 12.1 | 37. | 2.5 | 67. | 191. | 6.4 | 0.0 | -1.00 | -1.30 |
| 2316.0 | 2316.6 | C | 39.2 | 34. | 2.6 | 65. | 194. | 6.4 | 0.0 | -4.10 | -4.20 |
| 2322.0 | 2322.7 | C | 14.4 | 56. | 2.7 | 66. | 192. | 6.5 | 0.0 | -0.90 | -1.70 |
| 2325.6 | 2326.0 | C | 11.1 | 49. | 2.7 | 68. | 198. | 6.5 | 0.0 | -0.90 | -1.30 |
| 2328.0 | 2328.5 | C | 11.3 | 45. | 2.7 | 69. | 195. | 6.5 | 0.0 | -0.90 | -1.30 |
| 2330.6 | 2330.7 | C | 11.7 | 38. | 2.7 | 68. | 193. | 6.5 | 0.0 | -1.00 | -1.30 |
| 2333.6 | 2334.3 | C | 10.3 | 302. | 2.7 | 67. | 193. | 6.5 | 0.0 | -0.50 | 0.30 |
| 2339.0 | 2340.0 | C | 13.1 | 5. | 2.7 | 71. | 198. | 6.3 | 0.0 | -1.30 | -0.80 |
| 2340.0 | 2341.0 | C | 14.0 | 29. | 2.7 | 71. | 197. | 6.3 | 0.0 | -1.30 | -1.30 |
| 2345.0 | 2345.7 | C | 30.7 | 63. | 2.8 | 70. | 199. | 6.2 | 0.0 | -2.00 | -3.50 |
| 2352.0 | 2352.3 | C | 21.9 | 52. | 2.5 | 69. | 200. | 6.2 | 0.0 | -1.70 | -2.30 |

| CORRELATION INTERVAL | | CORR. GRADE | DIP ANGLE | DIP AZ. | DRFT ANGLE | DRFT AZ. | DIA NO.1 | DIA 13 | DISPLACEMENTS NO.1 | NO.2 | NO.3 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 2354.0 | 2354.3 | B | 23.3 | 41. | 2.5 | 70. | 197. | 6.2 | 0.0 | -2.00 | -2.30 |
| 2357.3 | 2357.4 | C | 10.7 | 0. | 2.4 | 72. | 189. | 6.2 | 0.0 | -1.00 | -0.70 |
| 2362.0 | 2364.0 | D | 28.2 | 61. | 2.5 | 72. | 202. | 6.2 | 0.0 | -2.00 | -3.10 |
| 2374.0 | 2374.4 | C | 33.2 | 51. | 2.6 | 74. | 194. | 6.2 | 0.0 | -2.50 | -3.70 |
| 2377.6 | 2378.0 | C | 21.4 | 55. | 2.4 | 74. | 192. | 6.2 | 0.0 | -1.30 | -2.30 |
| 2381.0 | 2382.0 | C | 15.8 | 11. | 2.4 | 75. | 163. | 6.2 | 0.0 | -1.10 | -1.50 |
| 2385.0 | 2385.7 | C | 16.8 | 23. | 2.6 | 77. | 154. | 6.2 | 0.0 | -0.70 | -1.70 |
| 2392.0 | 2393.0 | C | 19.1 | 22. | 2.6 | 80. | 160. | 6.1 | 0.0 | -1.00 | -1.90 |
| 2395.0 | 2396.0 | C | 26.8 | 345. | 2.6 | 80. | 167. | 6.1 | 0.0 | -2.50 | -1.70 |
| 2398.0 | 2399.0 | C | 13.7 | 61. | 2.7 | 79. | 166. | 6.1 | 0.0 | 0.0 | -1.30 |
| 2419.0 | 2420.0 | C | 13.2 | 347. | 2.6 | 75. | 242. | 6.2 | 0.0 | -0.70 | 0.50 |
| 2425.0 | 2425.3 | C | 19.9 | 13. | 2.7 | 79. | 245. | 6.2 | 0.0 | -1.60 | 0.20 |
| 2426.0 | 2428.0 | C | 8.5 | 15. | 2.7 | 77. | 244. | 6.2 | 0.0 | -0.80 | -0.10 |
| 2434.0 | 2435.0 | C | 33.7 | 348. | 2.6 | 81. | 241. | 6.1 | 0.0 | -1.70 | 1.70 |
| 2437.0 | 2438.0 | C | 22.2 | 324. | 2.7 | 79. | 248. | 6.1 | 0.0 | 0.0 | 1.70 |
| 2443.0 | 2444.0 | C | 29.6 | 8. | 2.6 | 81. | 253. | 6.2 | 0.0 | -1.90 | 1.10 |
| 2462.0 | 2464.0 | C | 21.2 | 11. | 2.7 | 85. | 169. | 6.1 | 0.0 | -1.60 | -1.90 |
| 2484.0 | 2486.0 | C | 19.3 | 24. | 2.8 | 83. | 109. | 6.1 | 0.0 | 0.70 | -1.20 |
| 2488.0 | 2489.0 | C | 6.0 | 81. | 2.8 | 82. | 105. | 6.1 | 0.0 | 0.80 | 0.30 |
| 2511.6 | 2511.7 | C | 20.2 | 28. | 2.7 | 84. | 131. | 6.1 | 0.0 | 0.10 | -1.70 |
| 2516.0 | 2516.6 | B | 15.9 | 29. | 2.8 | 85. | 148. | 6.1 | 0.0 | -0.30 | -1.50 |
| 2524.0 | 2524.7 | B | 16.5 | 18. | 2.8 | 87. | 137. | 6.1 | 0.0 | -0.30 | -1.50 |
| 2527.0 | 2528.0 | B | 20.5 | 50. | 2.7 | 87. | 152. | 6.1 | 0.0 | 0.10 | -1.80 |
| 2530.0 | 2530.5 | B | 22.6 | 46. | 2.6 | 85. | 155. | 6.0 | 0.0 | -0.20 | -2.10 |
| 2535.0 | 2536.0 | C | 11.4 | 34. | 2.6 | 87. | 189. | 6.0 | 0.0 | -0.80 | -1.10 |
| 2539.0 | 2539.4 | C | 18.9 | 11. | 2.5 | 87. | 174. | 6.1 | 0.0 | -1.50 | -1.60 |
| 2542.0 | 2543.0 | B | 15.3 | 28. | 2.5 | 87. | 155. | 6.2 | 0.0 | -0.50 | -1.50 |
| 2570.0 | 2572.0 | C | 21.0 | 357. | 2.4 | 91. | 162. | 6.2 | 0.0 | -1.70 | -1.70 |
| 2574.0 | 2576.0 | C | 24.6 | 341. | 2.3 | 89. | 157. | 6.2 | 0.0 | -2.20 | -1.70 |
| 2585.0 | 2586.0 | C | 17.9 | 23. | 2.4 | 85. | 176. | 6.2 | 0.0 | -1.30 | -1.70 |
| 2587.0 | 2588.0 | C | 15.0 | 15. | 2.4 | 86. | 187. | 6.2 | 0.0 | -1.30 | -1.20 |
| 2591.0 | 2592.0 | C | 11.0 | 23. | 2.4 | 90. | 173. | 6.4 | 0.0 | -0.70 | -1.10 |
| 2598.0 | 2600.0 | C | 27.4 | 8. | 2.4 | 89. | 150. | 6.2 | 0.0 | -1.70 | -2.70 |
| 2624.0 | 2626.0 | C | 8.4 | 43. | 2.3 | 89. | 181. | 6.2 | 0.0 | -0.40 | -0.90 |
| 2638.0 | 2640.0 | D | 34.3 | 316. | 2.1 | 84. | 124. | 6.1 | 0.0 | -3.10 | -2.70 |
| 2658.0 | 2660.0 | C | 12.9 | 232. | 2.5 | 93. | 125. | 6.2 | 0.0 | -0.30 | 0.80 |
| 2660.0 | 2662.0 | C | 14.0 | 30. | 2.4 | 94. | 126. | 6.1 | 0.0 | 0.30 | -1.00 |
| 2666.0 | 2668.0 | C | 23.8 | 315. | 2.4 | 92. | 122. | 6.1 | 0.0 | -1.90 | -1.70 |
| 2671.3 | 2672.0 | C | 30.2 | 344. | 2.2 | 92. | 138. | 6.1 | 0.0 | -2.30 | -2.70 |
| 2694.0 | 2695.0 | C | 18.4 | 33. | 2.4 | 92. | 189. | 6.1 | 0.0 | -1.40 | -1.70 |
| 2705.7 | 2706.0 | B | 17.4 | 32. | 2.1 | 91. | 225. | 6.1 | 0.0 | -1.70 | -0.90 |
| 2711.0 | 2711.3 | C | 17.9 | 78. | 2.2 | 87. | 265. | 6.1 | 0.0 | -1.90 | -1.10 |
| 2722.0 | 2722.8 | C | 17.1 | 66. | 2.4 | 96. | 281. | 6.2 | 0.0 | -1.70 | -0.30 |
| 2729.6 | 2730.0 | B | 11.0 | 52. | 2.2 | 95. | 265. | 6.1 | 0.0 | -1.10 | -0.30 |
| 2733.0 | 2734.0 | C | 22.1 | 48. | 2.2 | 94. | 249. | 6.3 | 0.0 | -2.30 | -0.90 |
| 2735.0 | 2735.3 | B | 25.1 | 40. | 2.2 | 95. | 246. | 6.4 | 0.0 | -2.60 | -0.80 |
| 2739.0 | 2740.0 | C | 32.3 | 59. | 2.2 | 96. | 241. | 6.2 | 0.0 | -3.50 | -2.30 |
| 2770.0 | 2771.0 | C | 10.9 | 50. | 2.1 | 101. | 252. | 6.1 | 0.0 | -1.10 | -0.50 |
| 2775.0 | 2776.0 | C | 1.6 | 227. | 2.0 | 100. | 234. | 6.1 | 0.0 | 0.10 | -0.10 |
| 2788.0 | 2789.0 | C | 17.4 | 27. | 2.1 | 94. | 214. | 5.9 | 0.0 | -1.60 | -1.00 |
| 2792.0 | 2794.0 | C | 8.4 | 88. | 2.0 | 95. | 233. | 5.9 | 0.0 | -0.60 | -0.90 |
| 2795.0 | 2795.3 | C | 20.1 | 32. | 2.0 | 94. | 221. | 5.9 | 0.0 | -1.90 | -1.10 |
| 2800.0 | 2800.3 | B | 6.4 | 56. | 1.9 | 95. | 193. | 6.1 | 0.0 | -0.30 | -0.70 |
| 2804.0 | 2804.3 | C | 10.9 | 16. | 2.0 | 95. | 180. | 6.0 | 0.0 | -0.80 | -0.90 |
| 2806.0 | 2806.4 | C | 17.0 | 342. | 2.2 | 96. | 167. | 5.9 | 0.0 | -1.40 | -0.90 |

| CORRELATION INTERVAL | | CORR. GRADE | DIP ANGLE | DIP AZ. | DRFT ANGLE | DRFT AZ. | AZ. NO.1 | DIA 13 | DISPLACEMENTS NO.1 | NO.2 | NO.3 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 2837.0 | 2838.0 | C | 12.4 | 1. | 2.1 | 92. | 125. | 6.3 | 0.0 | -0.30 | -1.10 |
| 2842.0 | 2844.0 | D | 6.4 | 181. | 2.2 | 100. | 102. | 6.1 | 0.0 | 0.20 | 0.70 |
| 2852.0 | 2852.3 | C | 13.3 | 357. | 2.4 | 99. | 84. | 6.0 | 0.0 | 0.40 | -0.70 |
| 2859.0 | 2860.0 | C | 12.4 | 15. | 2.1 | 99. | 118. | 6.0 | 0.0 | 0.10 | -0.90 |
| 2862.0 | 2862.3 | C | 6.6 | 359. | 2.1 | 98. | 127. | 6.0 | 0.0 | -0.10 | -0.50 |
| 2885.2 | 2885.3 | C | 18.2 | 14. | 1.7 | 98. | 122. | 6.0 | 0.0 | -0.10 | -1.50 |
| 2896.0 | 2896.3 | B | 17.9 | 11. | 1.8 | 92. | 119. | 6.1 | 0.0 | -0.10 | -1.50 |
| 2899.0 | 2900.0 | C | 14.0 | 30. | 1.9 | 99. | 132. | 6.1 | 0.0 | 0.10 | -1.10 |
| 2907.0 | 2907.2 | C | 13.8 | 287. | 1.9 | 98. | 117. | 6.0 | 0.0 | -1.10 | -0.50 |
| 2911.6 | 2912.0 | C | 13.5 | 260. | 1.8 | 100. | 119. | 5.9 | 0.0 | -0.90 | 0.10 |
| 2918.0 | 2918.6 | C | 11.3 | 339. | 1.7 | 98. | 118. | 5.9 | 0.0 | -0.50 | -0.90 |
| 2925.6 | 2925.9 | B | 33.2 | 330. | 1.6 | 94. | 127. | 6.0 | 0.0 | -2.70 | -2.90 |
| 2927.0 | 2928.0 | C | 19.6 | 12. | 1.5 | 96. | 138. | 6.0 | 0.0 | -0.70 | -1.80 |
| 2930.0 | 2931.0 | B | 27.8 | 24. | 1.5 | 98. | 142. | 6.1 | 0.0 | -0.80 | -2.70 |
| 2937.7 | 2938.2 | C | 23.6 | 41. | 1.5 | 89. | 146. | 6.1 | 0.0 | -0.10 | -2.10 |
| 2946.0 | 2946.3 | C | 3.6 | 86. | 1.6 | 95. | 134. | 6.0 | 0.0 | 0.40 | 0.0 |
| 2950.0 | 2950.6 | C | 21.7 | 38. | 1.6 | 90. | 135. | 5.9 | 0.0 | 0.20 | -1.70 |
| 2953.8 | 2954.0 | C | 24.5 | 58. | 1.5 | 91. | 186. | 6.1 | 0.0 | -1.10 | -2.50 |
| 2957.0 | 2957.2 | C | 5.1 | 105. | 1.5 | 90. | 186. | 6.1 | 0.0 | 0.20 | -0.40 |
| 2959.6 | 2960.0 | C | 18.1 | 105. | 1.6 | 92. | 189. | 6.0 | 0.0 | 0.50 | -1.30 |
| 2965.6 | 2966.0 | C | 18.3 | 353. | 1.5 | 93. | 153. | 6.1 | 0.0 | -1.40 | -1.50 |
| 2970.0 | 2970.6 | B | 17.4 | 35. | 1.5 | 90. | 149. | 6.1 | 0.0 | -0.30 | -1.60 |
| 2972.0 | 2972.5 | B | 9.9 | 354. | 1.5 | 90. | 155. | 6.1 | 0.0 | -0.70 | -0.80 |
| 2974.0 | 2974.6 | C | 13.8 | 71. | 1.5 | 87. | 153. | 6.1 | 0.0 | 0.50 | -0.90 |
| 2977.6 | 2978.0 | C | 17.8 | 20. | 1.5 | 91. | 163. | 6.2 | 0.0 | -1.10 | -1.70 |
| 2986.0 | 2986.5 | C | 22.0 | 291. | 1.5 | 85. | 177. | 6.2 | 0.0 | -1.10 | 0.90 |
| 2990.6 | 2992.0 | C | 14.4 | 340. | 1.4 | 88. | 217. | 6.0 | 0.0 | -0.90 | 0.30 |
| 2995.7 | 2996.3 | C | 11.9 | 33. | 1.3 | 87. | 208. | 6.2 | 0.0 | -1.10 | -0.90 |
| 3002.3 | 3003.0 | B | 10.5 | 32. | 1.3 | 83. | 240. | 6.1 | 0.0 | -1.00 | -0.30 |
| 3004.3 | 3005.0 | C | 8.1 | 357. | 1.3 | 86. | 241. | 6.1 | 0.0 | -0.50 | 0.20 |
| 3018.0 | 3018.4 | B | 35.5 | 327. | 1.3 | 86. | 189. | 6.1 | 0.0 | -3.10 | 0.10 |
| 3032.0 | 3033.0 | C | 15.4 | 26. | 1.3 | 75. | 217. | 6.1 | 0.0 | -1.50 | -0.80 |
| 3036.0 | 3037.0 | B | 24.3 | 149. | 1.5 | 77. | 225. | 6.2 | 0.0 | 0.90 | -1.60 |
| 3043.0 | 3044.0 | B | 11.2 | 24. | 1.6 | 75. | 223. | 6.1 | 0.0 | -1.10 | -0.50 |
| 3048.0 | 3048.5 | B | 4.3 | 59. | 1.5 | 71. | 237. | 6.2 | 0.0 | -0.50 | -0.40 |
| 3050.0 | 3050.5 | B | 14.2 | 35. | 1.5 | 71. | 238. | 6.1 | 0.0 | -1.40 | -0.50 |
| 3054.0 | 3054.6 | B | 13.4 | 69. | 1.6 | 72. | 222. | 6.1 | 0.0 | -1.10 | -1.30 |
| 3057.0 | 3058.0 | B | 16.4 | 47. | 1.7 | 72. | 220. | 6.2 | 0.0 | -1.60 | -1.30 |
| 3060.0 | 3060.3 | C | 14.8 | 308. | 1.6 | 77. | 179. | 6.2 | 0.0 | -1.00 | 0.20 |
| 3069.0 | 3070.0 | D | 2.7 | 260. | 1.6 | 71. | 164. | 6.4 | 0.0 | 0.0 | 0.10 |

THE FOLLOWING PARAMETERS APPLY TO THE LOG FROM 400.0 FEET TO 3070.0

MAGNETIC DECLINATION IS 21.0 DEGREES.